

# Simulation of Criticality Accident Transients in Uranyl Nitrate Solution with COMSOL Multiphysics

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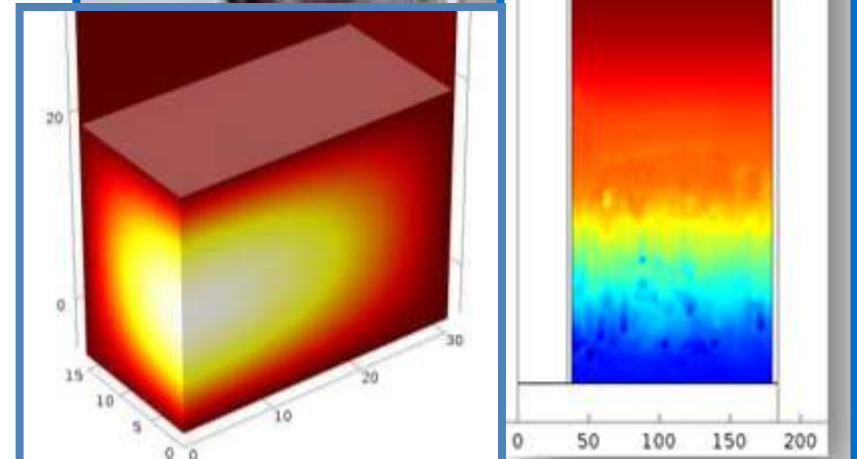
Y-12, Safety Analysis Engineering

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Presented at the



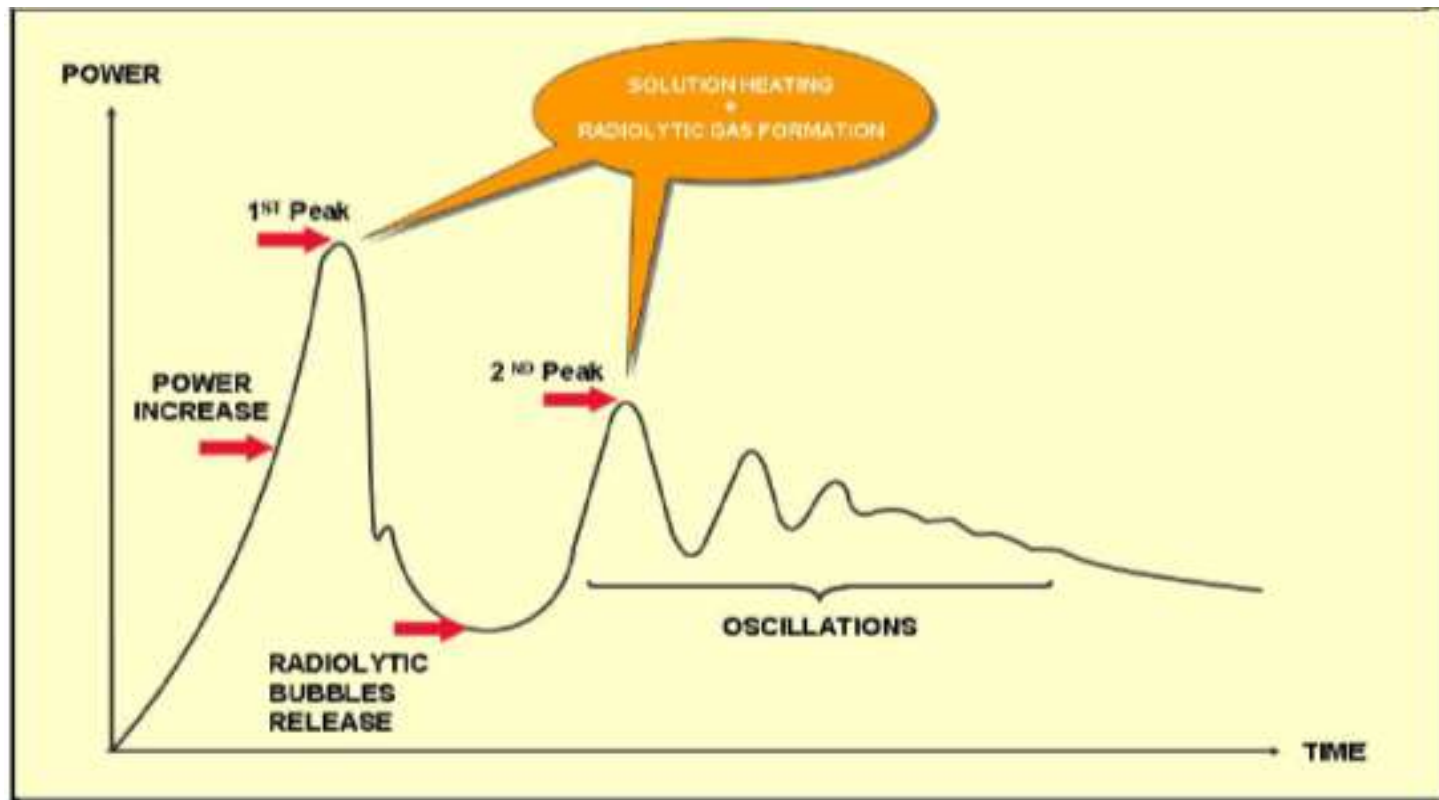
# Presentation Outline



- **Brief background**
- **Model Introduction**
- **Governing Equations**
  - Point Kinetics
  - Conjugate Heat Transfer
  - Radiolytic Gas Transport
- **Results**
  - SILENE benchmark
  - “Methodological” Exercise
- **Conclusions**

# Criticality Transients in Solution

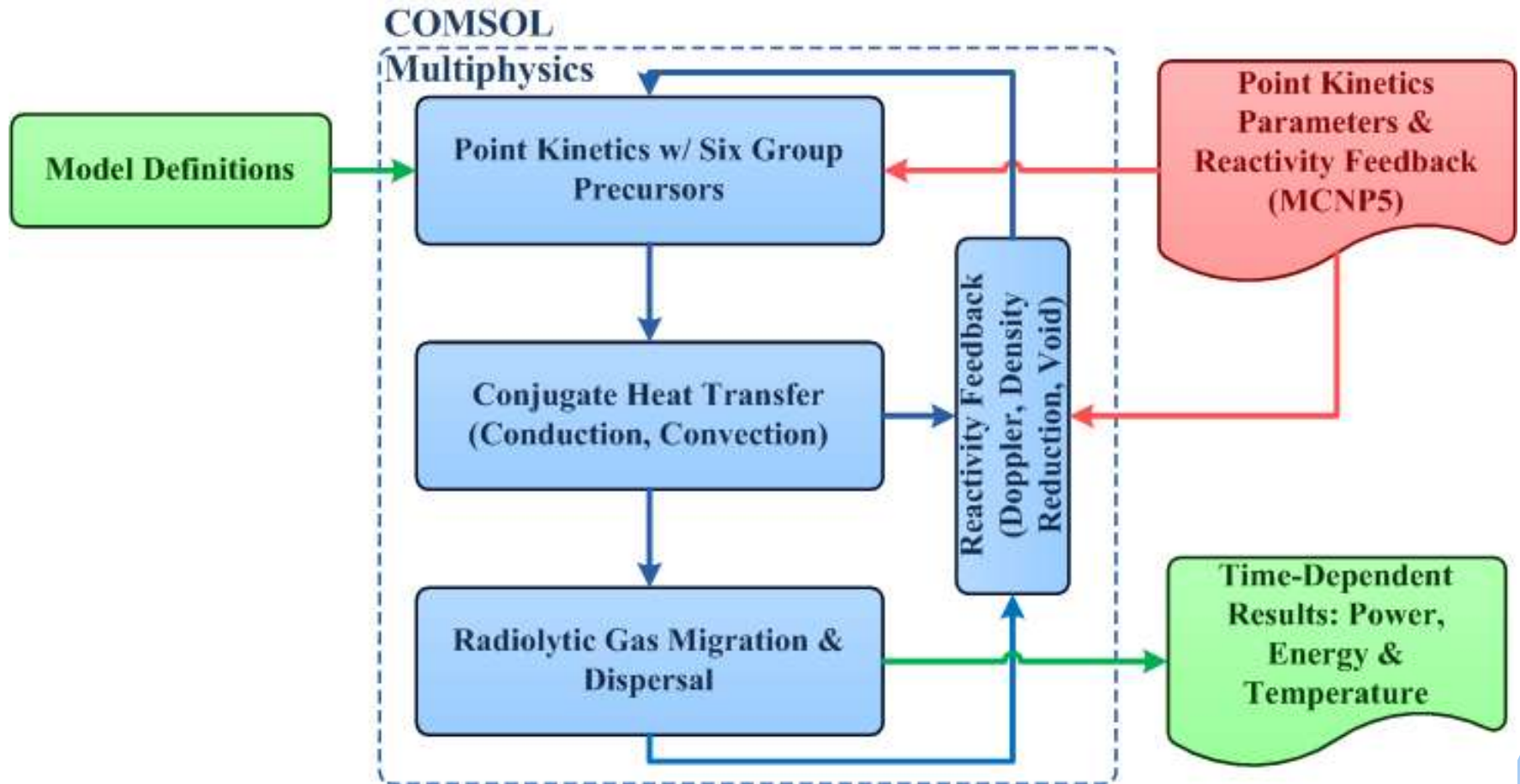
- **Typical Multiphysics Reactivity Feedbacks:**
  - Included in Model: Radiolytic Gas, Thermal Expansion, Temperature (Cross Sections)
  - Not included: Solution Ejection, Sloshing, Boiling, etc.



# Model Introduction

- **Importance:**
  - Fissile solution transients often introduce a strongly time-dependent radiation source term for emergency planning, characterization of which is motivated by ANSI/ANS-8.23-2007, *Nuclear Criticality Accident Emergency Planning and Response*.
  - LA-13638 R2000, *A Review of Criticality Accidents* documents the nature and high frequency of process accidents in fissile solution or slurry.
- **Purpose: Develop a “Level 1.5” model of criticality transients in solution**
  - Serve as flexible & powerful intermediary between “Level 2” models with full radiation transport & CFD (FETCH) and less exhaustive “Level 1” models (AGNES, CRITEX, TRACE)

# Multiphysics Model Structure



# Point Kinetics

## Neutron Kinetics Balance

$$\frac{dP(t)}{dt} = \frac{\rho(t) - \beta_{eff}}{\Lambda} P(t) + \sum_{i=1}^6 \lambda_i C_i(t)$$

## Delayed Neutron Precursor Concentration

$$\frac{dC_i(t)}{dt} = \frac{\beta_i}{\Lambda} n(t) - \lambda_i C_i(t) \quad i = 1:6$$

## Reactivity

$$\rho(t) = \rho_0 + ramp(t) + \alpha_T \Delta T + \alpha_V \Delta V$$

$T$  temperature

$V$  void volume

$$\alpha_k = \frac{\partial \rho}{\partial k}$$

$P$  fission rate (fission/s)

$\rho$  reactivity

$\Lambda$  mean neutron generation time (s)

$C_i$  DNP concentration (neutrons/m<sup>3</sup>)

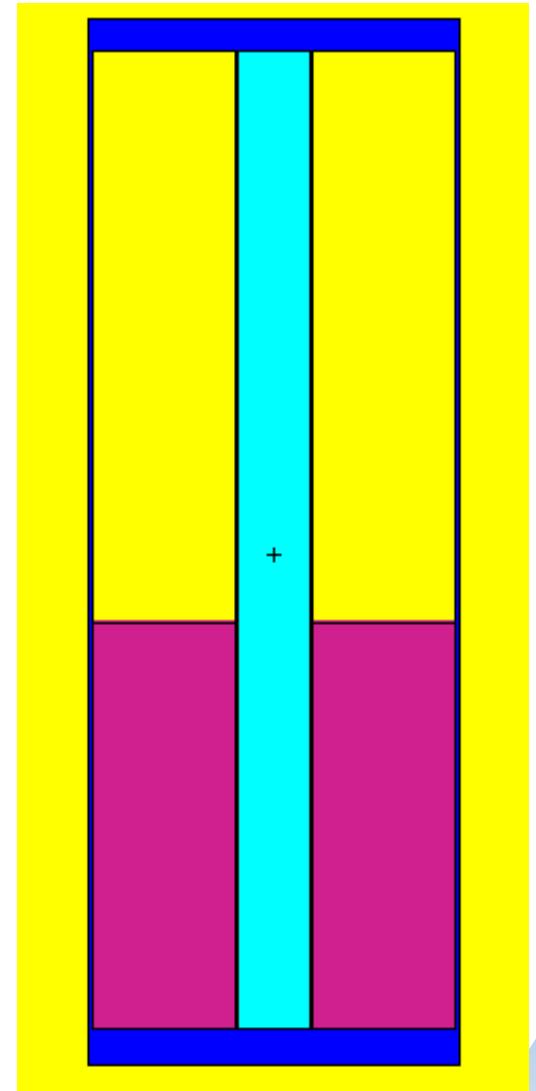
$\lambda_i$  decay constant (1/s)

$\beta_i$  delayed neutron fraction

$$\beta_{eff} = \sum_{i=1}^6 \beta_i$$

# Use of MCNP5

- **Point Kinetics Parameters**
  - Using MCNP5-1.6's KOPTS card precursor decay rates and delayed neutron fractions ( $\lambda_i$ 's &  $\beta_i$ 's) along with mean neutron generation time ( $\Lambda$ ) can be calculated using
- **Reactivity Feedback**
  - Step changes in reactivity vs. feedback parameters (void, temperature) are used to inform reactivity feedback coefficients ( $\alpha_k$ 's)



# Point Kinetics

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MCNP5

KOPTS card



# Conjugate Heat Transfer

## Heat Conduction & Convection

$$\dot{\rho} C_p \left( \frac{\partial T}{\partial t} + u \cdot \nabla T \right) = \nabla \cdot (k \nabla T) + Q$$

$T$  temperature (K)

$u$  fluid velocity (m/s)

$t$  time (s)

$Q$  volumetric heat source (W/m<sup>3</sup>)

$\dot{\rho}$  material density (kg/m<sup>3</sup>)

$k$  material thermal conductivity (W/m-K)

$C_p$  material specific heat capacity (W/kg-K)

## Volumetric Heat Source

$$Q = \frac{P w_e}{V} \prod_{i=1}^n \cos \left( \frac{\pi x_i}{L_i} - \delta_i \right)$$

$P$  power (fission/s)

$w_e$  fission energy release (J/fission)

$V$  fissile solution volume (m<sup>3</sup>)

$x_i, L_i, \delta_i$   $i^{\text{th}}$  dimensional position (m), length (m) and phase shift

## B.C.'s

- Heat continuity at internal boundaries
- Natural Convection to air at external boundaries
- Insulation/Symmetry at center boundaries

# Conjugate Heat Transfer (cont'd)

## Incompressible Navier-Stokes momentum

$$\dot{\rho} \left( \frac{\partial u}{\partial t} + (u \cdot \nabla)u \right) = -\nabla p + \nabla \left( \mu (\nabla u + (\nabla u)^T) - \frac{2}{3} \mu (\nabla \cdot u) I \right) + F$$

$p$  pressure (Pa)

$\mu$  material dynamic viscosity (Pa-s)

$F$  external body force (N/m<sup>3</sup>)

## Mass Continuity

$$\frac{\partial \dot{\rho}}{\partial t} + \nabla \cdot (\dot{\rho} u) = 0$$

## B.C.'s

- No slip at solution/container walls
- Outlet at external surface

# Radiolytic Gas Transport

## Radiolytic Gas Bubble Volume

$$\frac{\partial V}{\partial t} + (\mathbf{v} \cdot \nabla)V = v_e P(t) w_e (C - C_0) \theta(C - C_0)$$

$V$  bubble gas volume (m<sup>3</sup>)

$\mathbf{v}$  bubble velocity (m/s)

$v_e$  energy-void transfer coefficient (m<sup>6</sup>/mol-J)

$P$  power(fission/s)

$w_e$  energy released per fission=> (J/fission)

$\theta(x)$  heavyside function ( $x > 0 \rightarrow 1$ )

### B.C.'s

- Insulation/"Reflection" at container walls
- Outlet at solution surface

## Radiolytic Gas Concentration

$$\frac{\partial C}{\partial t} + (\mathbf{v} \cdot \nabla)C = G_H Q - \frac{C}{\tau}$$

$C$  radiolytic gas concentration (mol/m<sup>3</sup>)

$C_0$  saturation concentration (mol/m<sup>3</sup>)

$G_H$  gas molecular energy yield (mol/J)

$Q \propto P$  heat source (W/m<sup>3</sup>)

$\tau$  dissolution rate (s)

# COMSOL's built-in mesh generator used to discretize the geometry and Direct solvers are utilized

- Boundary layers in narrow domains located near steep flux gradients and/or fissile solution boundaries
  - “fine”-“extra fine” in core region (+refinements)
  - “coarse”-“normal” elsewhere
- Free triangular mesh elsewhere
  - ~20 thousand DOF → <12 hr solution time
  - 1 core computer, 4 GB RAM
- Direct Solver: COMSOL's MUMPS & PARDISIO algorithms
  - Extendable to multi-node parallel runs



# Transient: SILENE LE1-641

- **Background**

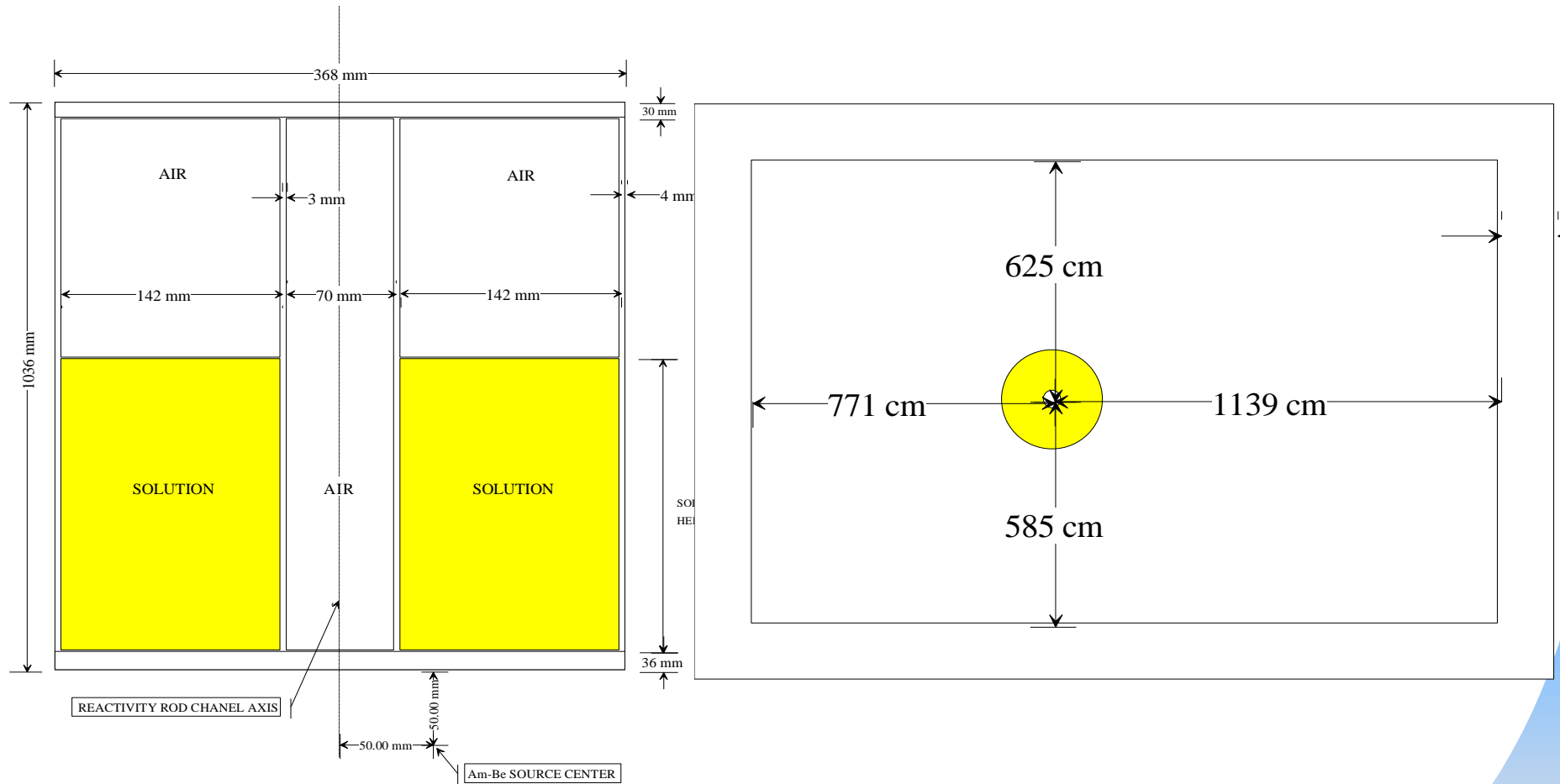
- Part of a series of criticality benchmarks performed at the Valduc facility in France
- Annular, cylindrical stainless steel reactor with control rod chamber
- 93% Enriched Uranyl Nitrate (~71 g U/I) Solution
- 2 \$ reactivity ramp over  $t=0:20$  seconds

- **Model**

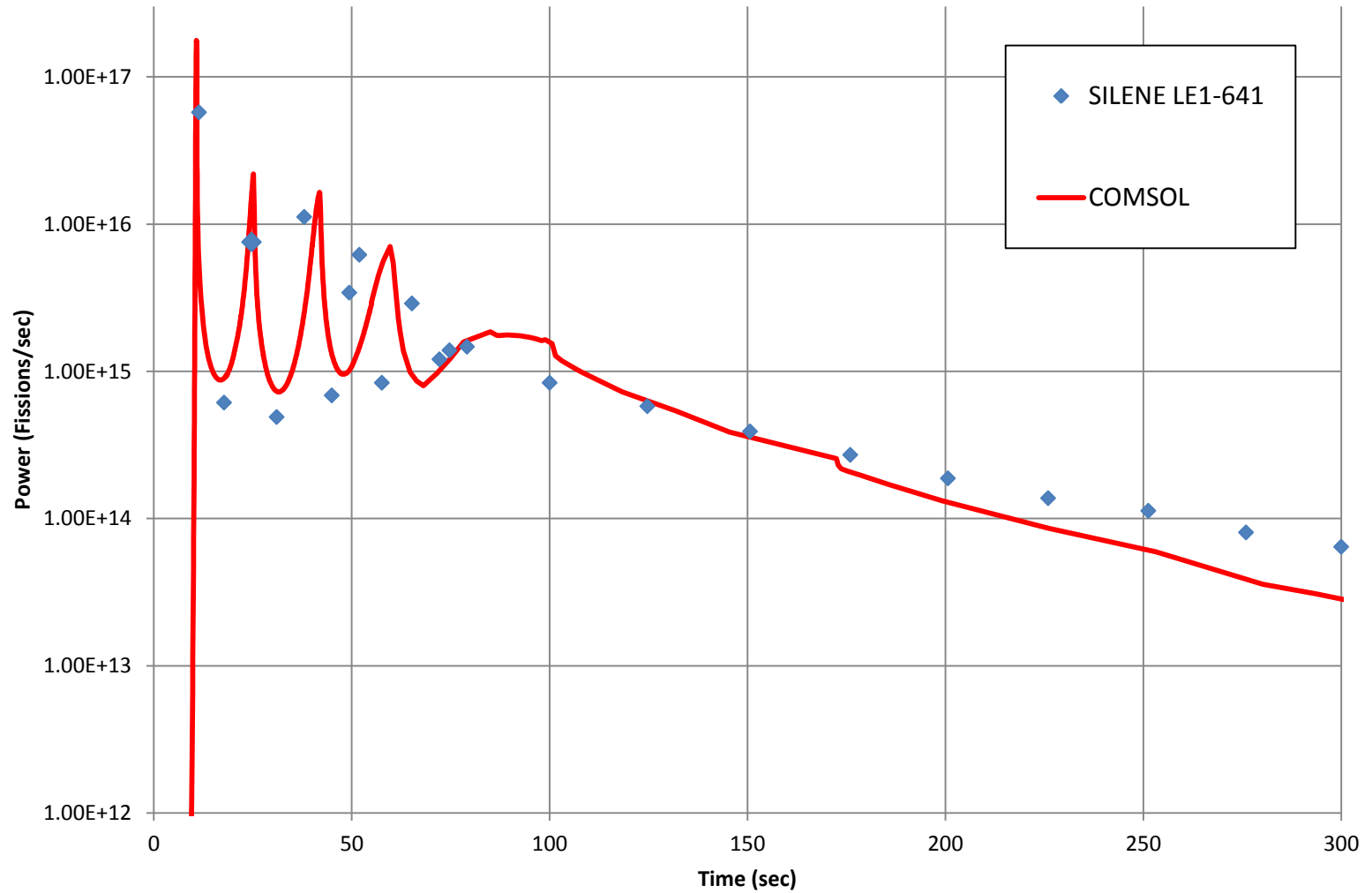
- 2-D Axisymmetric
- Variable time-stepping, error  $< 1e-2$



# Transient: SILENE LE1-641 (cont'd)

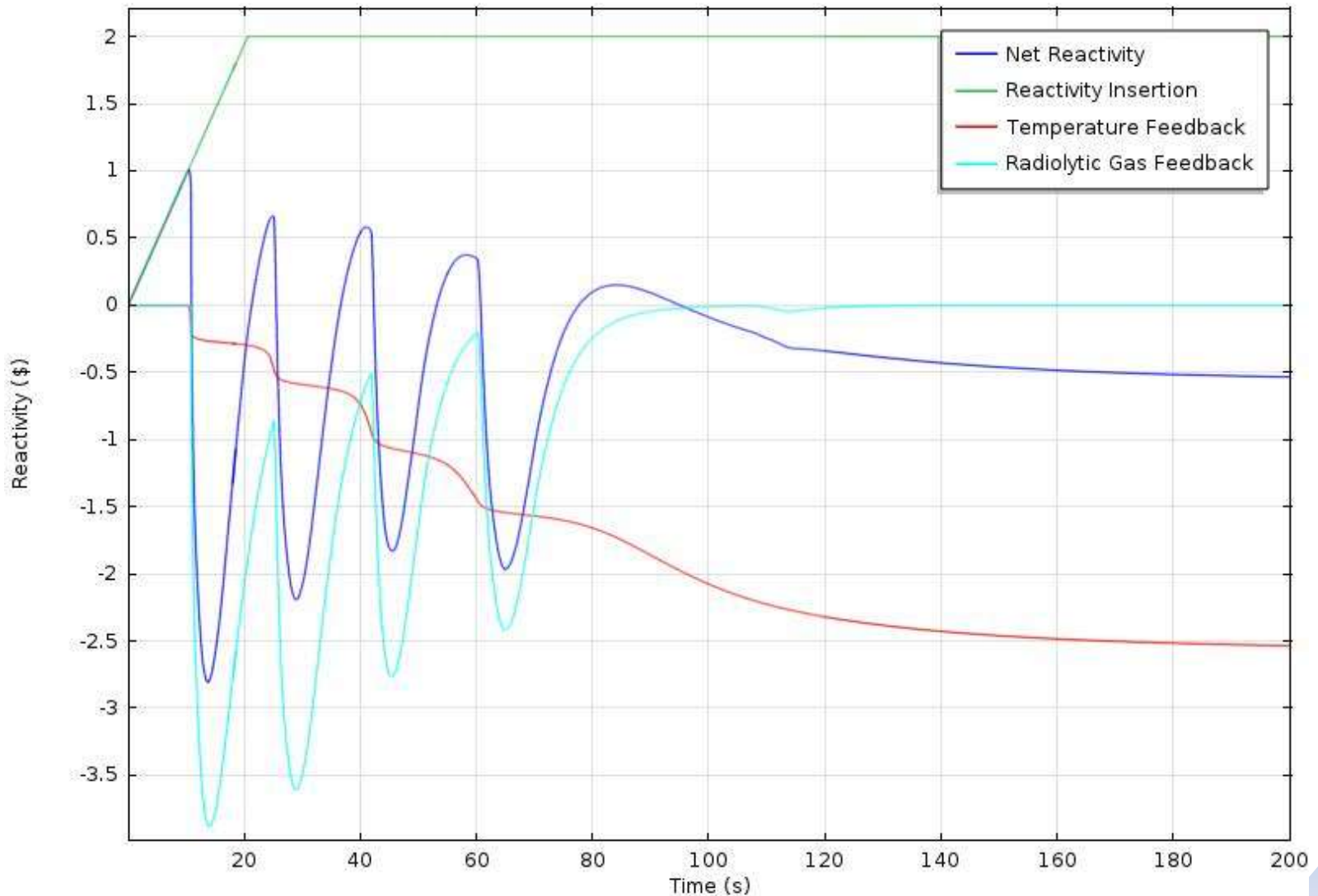


# Comparison to Benchmark



# SILENE LE1-641: Reactivity Contributions

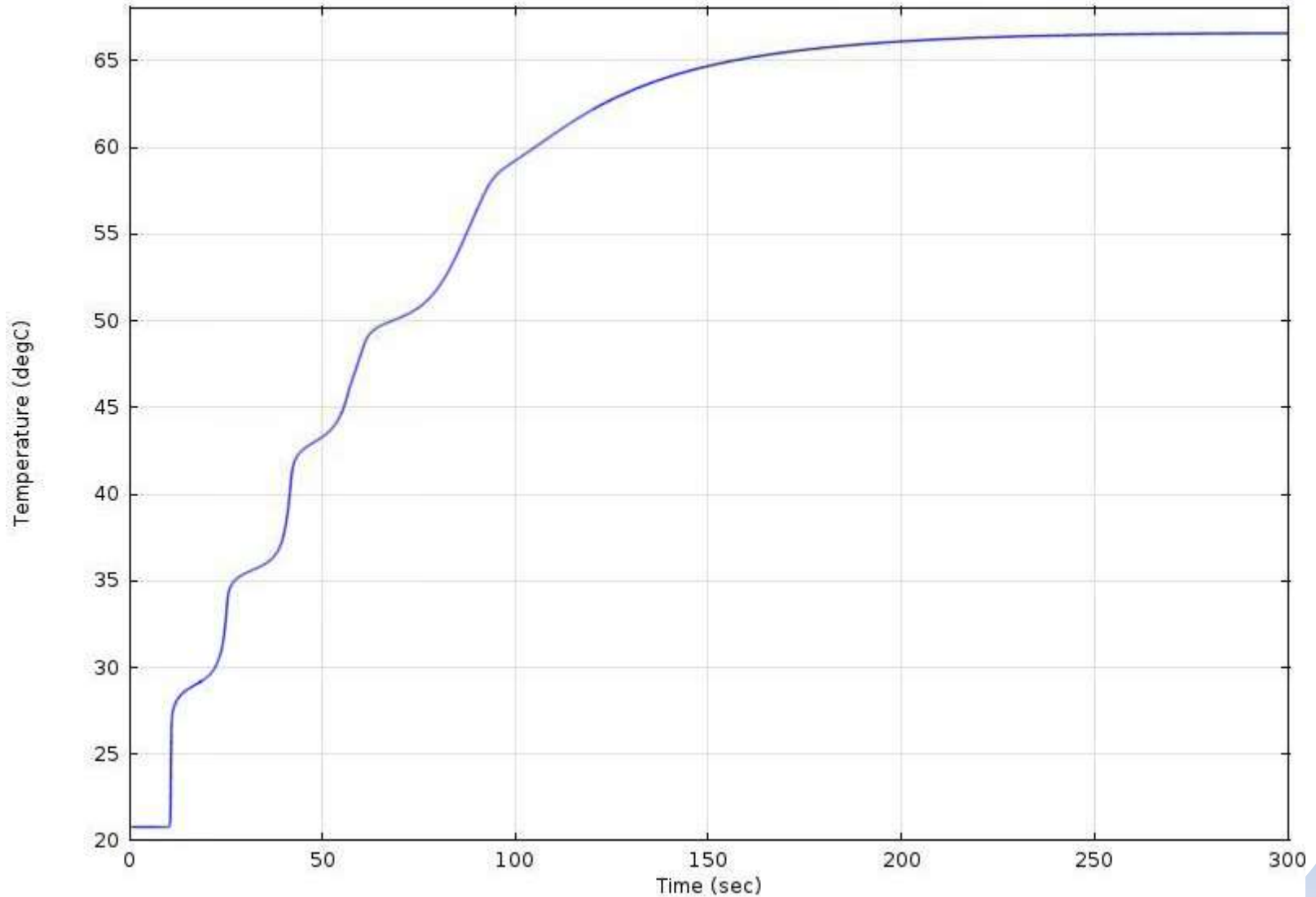
COMSOL MULTIPHYSICS



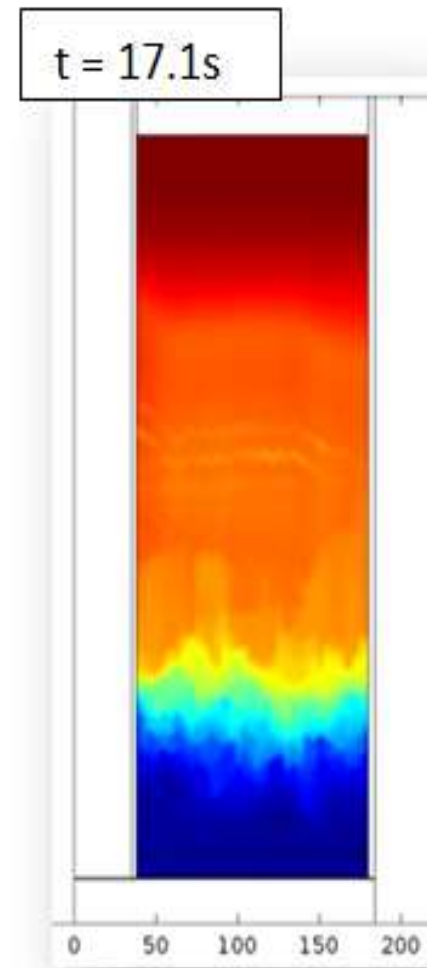
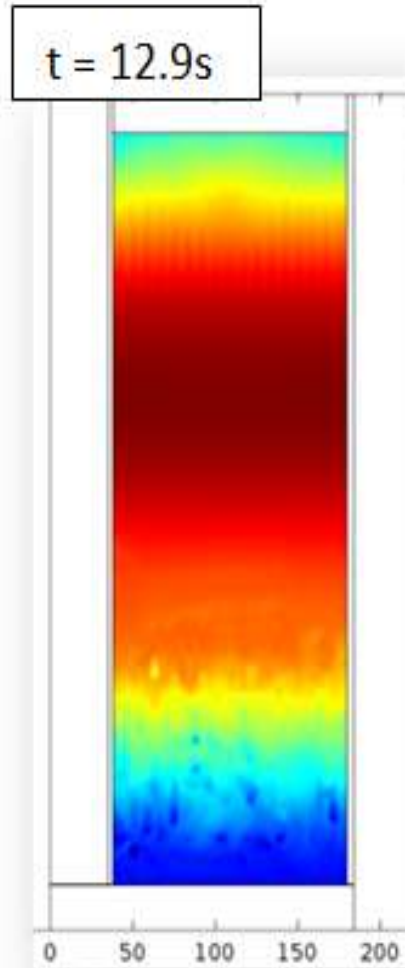
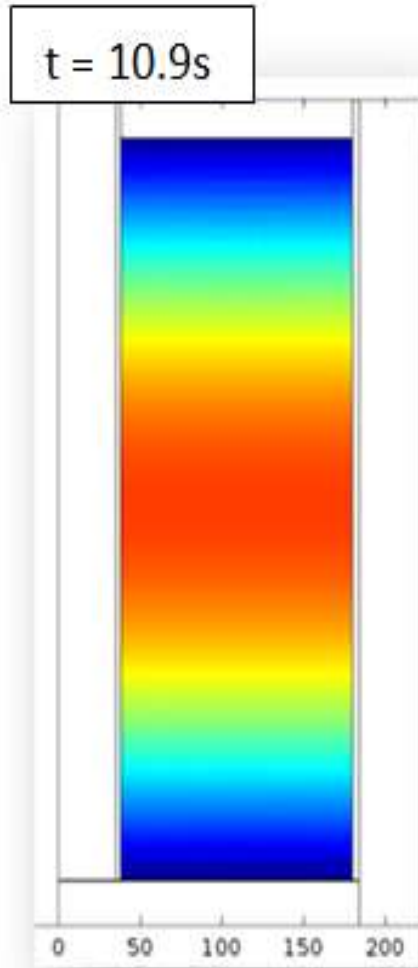


# SILENE LE1-641: Temperature

COMSOL  
MULTIPHYSICS

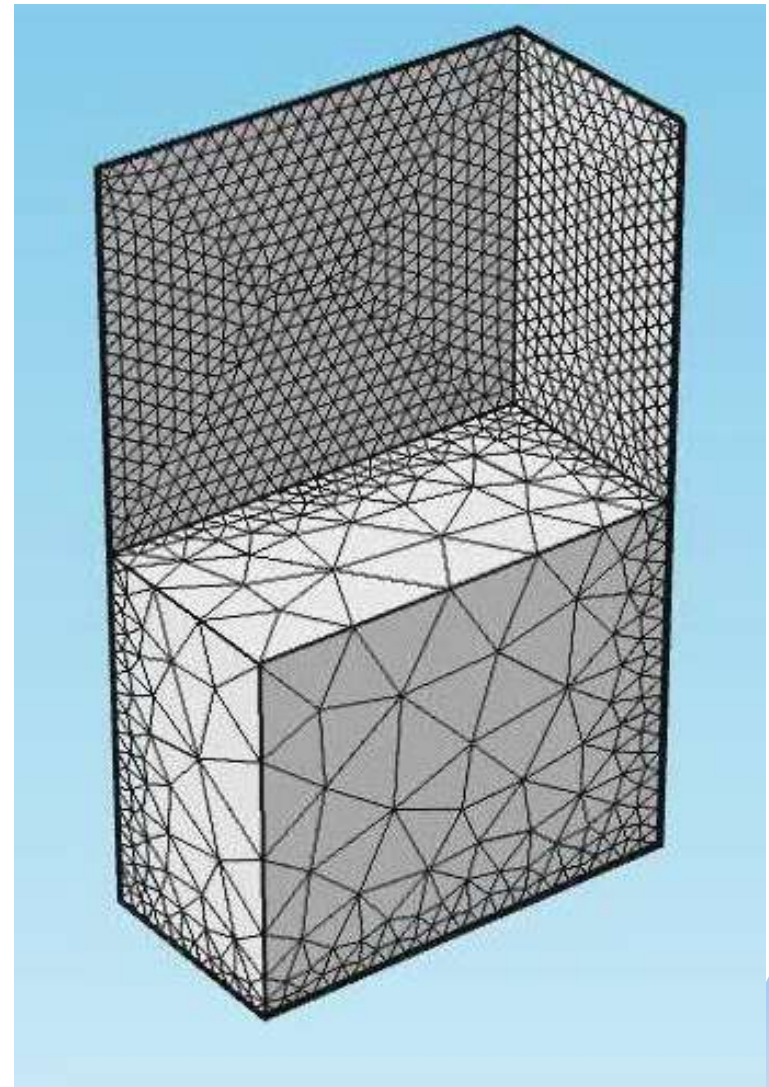
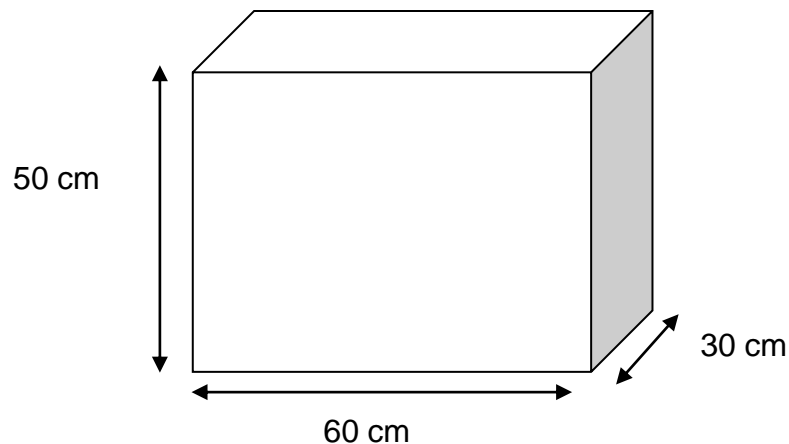


# Distribution of radiolytic gas around the first excursion peak



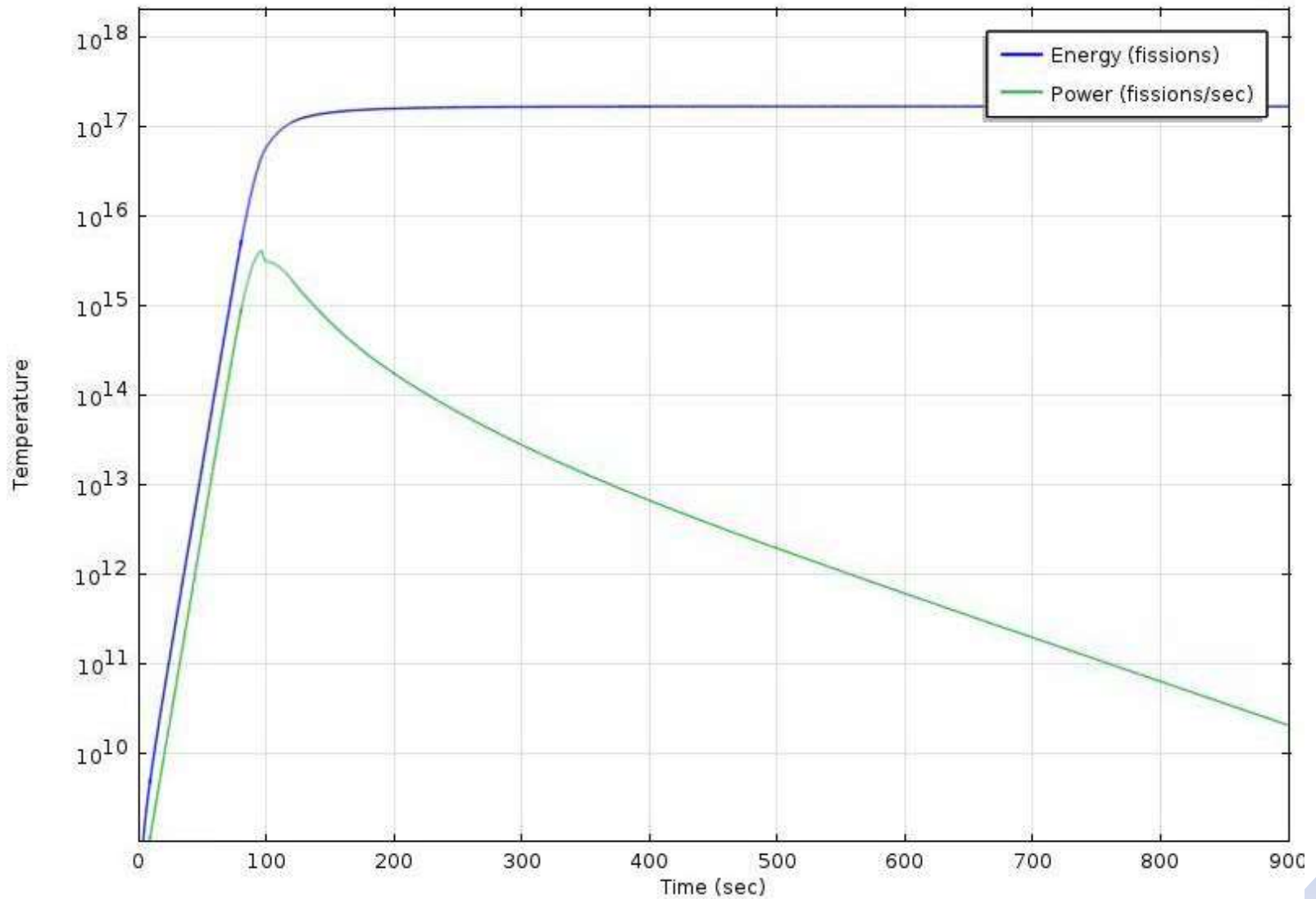
# Transient: “Methodological” Exercise

- Theoretical situation postulated by the OECD/NEA Criticality Excursion Analyses Experts Group at the 2011 International Conference on Nuclear Criticality
  - 93% Enriched Uranyl Nitrate (~71 g U/I) Solution
  - Rectangular stainless steel tank with no lid, surrounded by air
- COMSOL: 3-D quarter-slice, Error <  $1e-2$



# 50¢ Reactivity Step: Excursion History

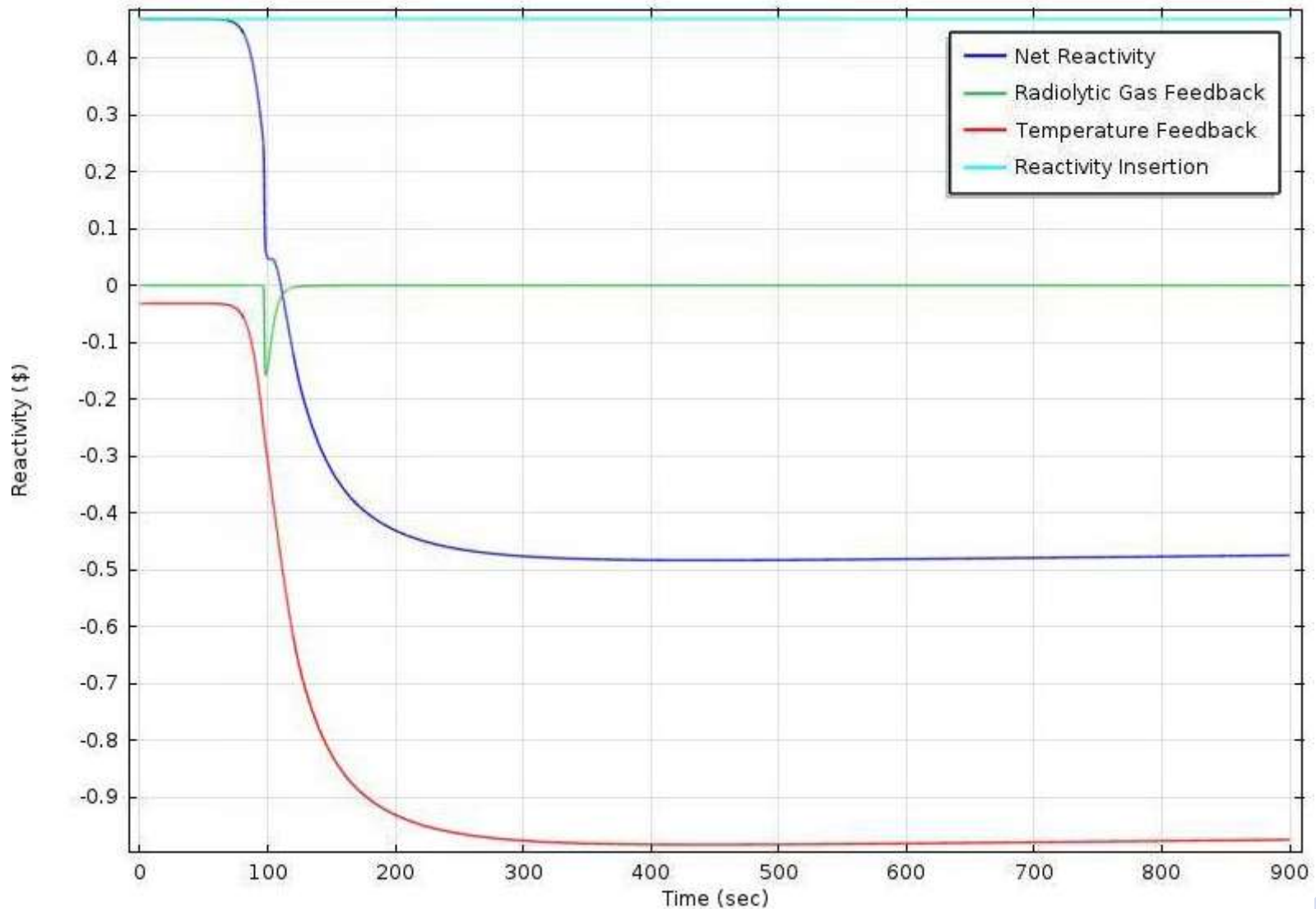
Exercise 1, 50 cent Step: Excursion Power History



# 50¢ Reactivity Step: Reactivity Feedback

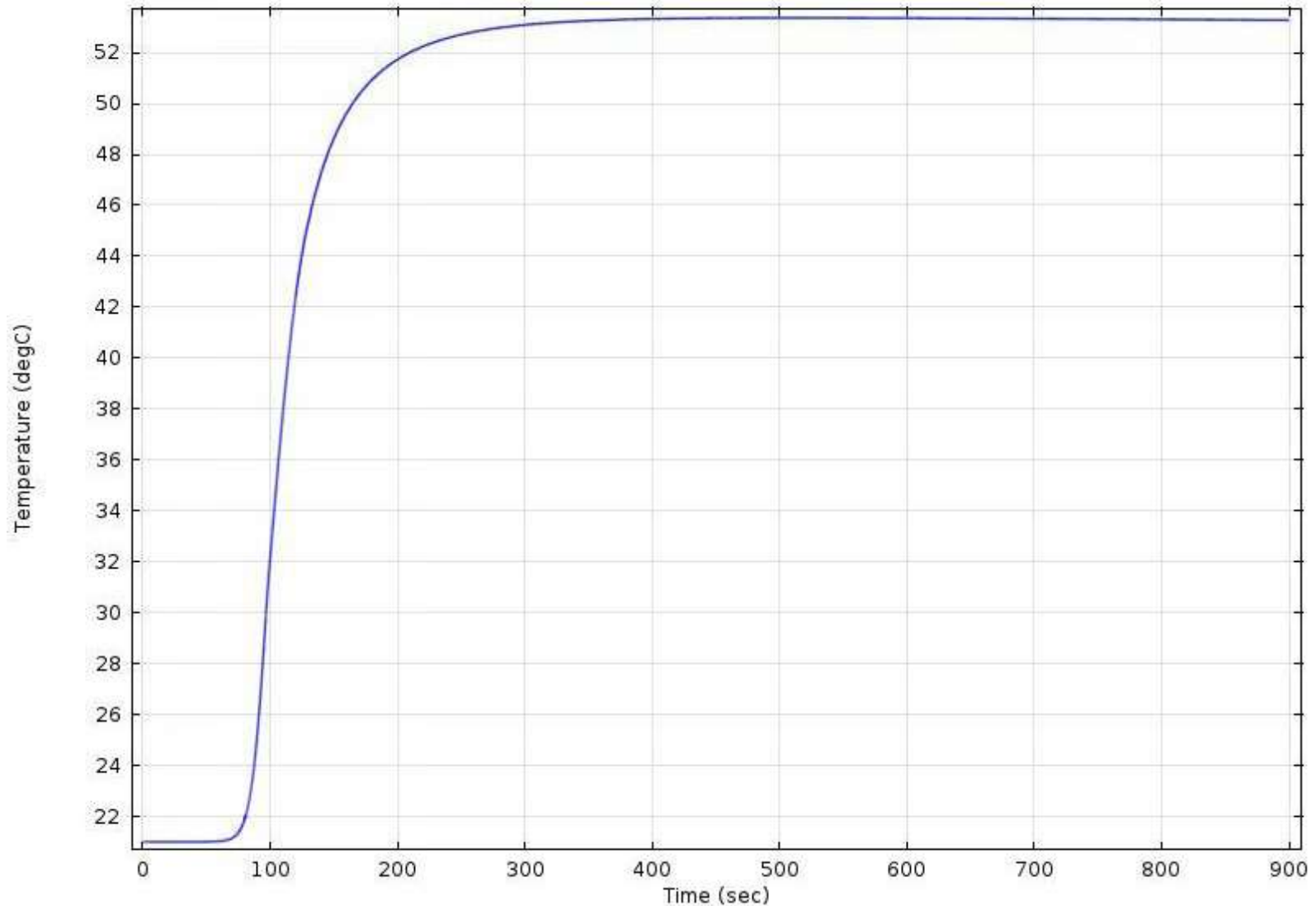
Exercise 1, 50 cent Step: Reactivity Contributions

CONTROL MULTIPHYSICS



# 50¢ Reactivity Step: Temperature

Exercise 1, 50 cent Step: Solution Temperature



# Summary and Conclusions

- **COMSOL-based models of UN solution transients were created via built-in & equation-based modeling**
  - 3 coupled physics phenomena: neutronics, conjugate heat transfer & radiolytic gas transport
  - 3-D & 2-D axisymmetric geometries
  - Nuclear data derived from MCNP5-1.60 & KOPTS card
- **Results are encouraging**
  - Expected power excursion behavior observed for all cases
  - Good agreement between referenced benchmark SILENE LE1-641
- **Plenty of room for improvement**
  - Solution Sloshing (surface distortion, moving mesh)
  - Space-time neutron kinetics methodology (few-group diffusion)
  - Extension to other benchmarks (different geometries & solutions)
  - Solution boiling

# Questions??

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