GE Hitachi Nuclear Energy

Monte Carlo Simulation of Fuel Pellet Spills with Axial Inter-Pellet Moderation and Stochastic Geometry

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Data, Analysis, and Operations in Nuclear Criticality Safety - I

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Overview

- Introduction
- Methodology
- Results
- Summary and Conclusions



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Introduction

- In LWR nuclear fuel manufacturing facilities, spills of UO₂ pellets are of concern to criticality safety.
- Occurrence of a criticality incident or accident depends on the mass, geometry and moderation involved in a pellet spill.
- Criticality safety assessment of pellet spills must be performed in accordance with the Double Contingency Principle.



Introduction (cont)

Consider a spill of sintered UO₂ pellets involving:

- 5 wt% U-235 fuel enrichment
- Hemispherical spill geometry involving 37 kg (safe mass of pellets).
- 12" concrete floor
- 12" water reflection on hemispherical surface
- Pellets modeled as rods (no axial spacing) or volumeequivalent spheres

Analyzed with MCNP5 in KCODE mode with 10⁶ active histories and standard deviation of about 0.0007.



4

Introduction (cont)

A) Array of rods



Hemispherical spill top and side crosssectional views.

B) Array of equivalent spheres









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Introduction (cont...)



Investigate effect of modeling pellets explicitly with axial spacing to isolate effect from sphere approximation.



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Methodology - Alternate arrangement of pellets in spills

Stochastic rods: Array of pellets arranged *nominally* as rods but each pellet located randomly in XY.

Type I (axial spaced): Array of pellets similar to the array of rods but adjacent pellets separated from each other in Z. Adjacent pellets are in-line in the Z direction.

Type II (offset axial spaced): Fully triangular-pitched array of pellets similar in arrangement to the array of spheres. Pellets are centered between three pellets in adjacent plane in Z.





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Methodology - Stochastic geometry in MCNP









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Methodology - Fully triangular pitched arrays



- An individual fuel pellet surrounded by water (*Universe 1*) is placed in an hexagonal prism and specified as a hexagonal lattice (lat=2) (*Universe 2*).
- A second hexagonal prism lattice is created translated by (x, x tan30, z) (*Universe 3*).
- Universe 2 is used to fill an infinite region defined by Planes 1 and 2 creating an infinite planar array of triangular-pitched pellets. Universe 3 is used to fill an infinite region defined by Planes 2 and 3. Together these two regions define Universe 4.
- Universe 4 is used to fill the region defined by planes 1 and 3, but using the square lattice (lat=1) and results in Universe 5.
- Universe 5, is used to fill the fuel region resulting in an array of triangular pitched pellets.



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Model description	Peak reactivity (k _{eff})	Reactivity for low W/F (k _{eff}) (W/F=0.577)
Array of rods (deterministic)	0.905	0.577
Equivalent volume spheres	0.930	n/a
Array of rods (stochastic pellets)	0.918	0.576
Type I model (axial spaced)	0.932	0.575
Type II model (offset axial spaced)	0.932	0.575



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Results – Axial spacing



Offset axial spaced pellets give an axial moderation effect even without axial spacing.



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Results – Pellet aspect

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Summary and conclusions

Dry conditions

• For low moderation conditions axial spacing had no effect.

Moderated conditions

- Limited stochastic treatment of array of pellets as rods gives an axial moderation effect but below models with explicit axial spacing.
- Array of equivalent volume spheres, or pellets with axial spacing (Type I or II), gave similar results and were the most conservative models.

Application

- If axial spacing at optimum moderation <u>is a credible condition</u>, axial spacing can be significant to safe operation.
- However for typical applications both conditions wouldn't exist simultaneously as pellets would be expected to spill into a relatively close-packed array resulting in low W/F. As the W/F effect is significantly greater than the axial spacing effect, the array of rods model remains conservative and considering axial spacing can be used for added conservatism.

