## List-Mode Simulations of the Subcritical Thor Core **Benchmark Sensitivity Experiments**

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Presented at the American Nuclear Society Winter Meeting in Anaheim, CA

November 11<sup>th</sup>. 2014

LA-UR-14-28651





### **General Overview**

- Sub-critical multiplying systems provide valuable information.
  - Validation of nuclear data and codes.
  - Uncertainty quantification for various applications.
  - Design of future measurements.
- Monte Carlo simulations of an experimental subcritical benchmark were performed.
  - Helps validate recent improvements in computational tools.
  - Provides better predictability and understanding in the sensitivities and uncertainties associated with subcritical systems.
- Experiments/simulations involved extensive mass and geometry perturbations.
  - 40+ different configurations: detailed model of the system & associated perturbations.
  - MCNP5 with list-mode patch used for simulations.
- ³He neutron multiplicity detectors provided list-mode data in exp. & simulation.
  - Time stamp (and location) of every registered event.
  - Data analyzed using the Feynman Variance-to-Mean method to obtain  $M_T$ .



### Subcritical System in Nevada: Thor Pu-metal core

- TA-18 operated at LANL from 1945-2005
  - 2004-2005: Shipment of nuclear material from TA-18 to DAF.
  - 2011: Critical experiment capability resumed at DAF.







- Assembled Thor pieces approximate a sphere ~10.6 cm in diameter.
  - Total net mass (with inserts) 9649.0 g.



Isotopic composition similar to Jezebel/BeRP.

5.1% <sup>240</sup>Pu (alloyed with ~1.01 wt% gallium), components clad with ~5 mils of Ni.

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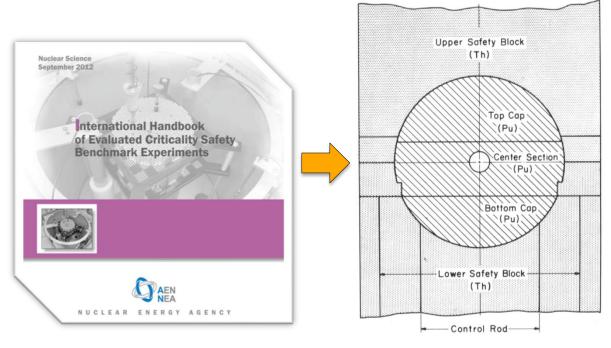
# Several major Thor Core experiment and evaluation publications are available in the literature.

NUCLEAR SCIENCE AND ENGINEERING: 71, 287-293 (1979)

#### Thor, A Thorium-Reflected Plutonium-Metal Critical Assembly

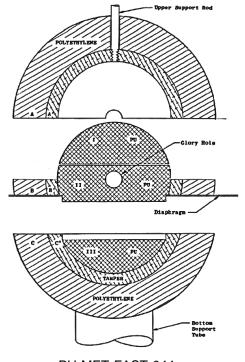
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Benchmark Critical Experiment of a Thorium Reflected Pu Sphere



PU-MET-FAST-044

Pu Metal Sphere with Be, Graphite, Al, Fe and Mo Tampers and Polyethylene Reflectors

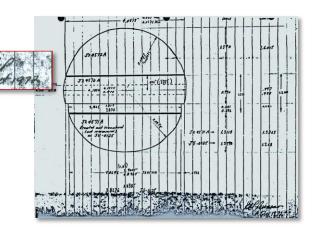


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# A geometry revaluation of the Thor core major components geometry was performed.

- Updated dimensions determined from:
  - Original unpublished drawings from 1972.
  - Unpublished documents from 2005 when material was transferred from Los Alamos to the Nevada National Security Site.
- Updated mass and density values also obtained for the Thor components from:
  - Mass measurements.
  - Stochastic volume ray-tracing estimation method with MCNP.
  - Analytical calculations.









## Updated Thor mass and volume from a recent geometry re-evaluation.

Coated [cm <sup>3</sup> ]	Ni [cm³]	Pu-alloy [cm³]	
206.4 ± 0.1	2.67 ± 0.01	203.7 ± 0.12	
Coated [g]	Ni [g]	Pu-alloy [g]	Pu [g]
$3273.9 \pm 0.1$	$23.78 \pm 0.1$	3249.2 ± 0.14	3216
3274.0	25.25	3249	3216.2
		3225	3192.4
		3225	3193
	206.4 ± 0.1  Coated [g]  3273.9 ± 0.1	206.4 ± 0.1 2.67 ± 0.01  Coated [g] Ni [g] 3273.9 ± 0.1 23.78 ± 0.1	$206.4 \pm 0.1$ $2.67 \pm 0.01$ $203.7 \pm 0.12$ Coated [g]Ni [g]Pu-alloy [g] $3273.9 \pm 0.1$ $23.78 \pm 0.1$ $3249.2 \pm 0.14$ $3274.0$ $25.25$ $3249$ $3225$



Center Component (JX-4570)				
Volume	Coated [cm <sup>3</sup> ]	Ni [cm³]	Pu-alloy [cm³]	
present work: MCNP5	$262.4 \pm 0.13$	$3.58 \pm 0.01$	258.8 ± 0.13	
Mass	Coated [g]	Ni [g]	Pu-alloy [g]	Pu [g]
present work: measurement / MCNP5	4158.2 ± 0.1	$31.9 \pm 0.1$	4126.3 ± 0.14	4085
unpublished work (2005)	4158.3	33.71	4124.6	4083
unpublished work (1972)			4127	4085.3
Robba et al. (1983)			4127	4086



Lower Spherical Cap (JU-125)				
Volume	Coated [cm <sup>3</sup> ]	Ni [cm³]	Pu-alloy [cm <sup>3</sup> ]	
present work: MCNP5	137.9 ± 0.1	2.22 ± 0.01	135.7 ± 0.1	
Mass	Coated [g]	Ni [g]	Pu-alloy [g]	Pu [g]
present work: measurement / MCNP5	2216.9 ± 0.1	19.7 ± 0.1	2197.2 ± 0.14	2175
unpublished work (2005)	2216.9	20.44	2196.5	2174.3
unpublished work (1972)	2216.75	20.85	2195.9	2173.7
Robba et al. (1983)			2196	2174





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## An updated Thor density of 15.95 g/cm<sup>3</sup> was obtained.

16.25

16.20

- Calculated  $\rho_{\text{Pu-alloy}}$  for Center/Upper components within statistical uncertainties.
  - Mass-averaged value of 15.95 g/cm<sup>3</sup>.
- Discrepancy in Lower piece.
  - Likely attributed to dimension inaccuracies.
  - Component was stripped of its original Ni cladding leading to material loss.
- Density of  $\delta$ -phase plutonium metal decreases as a function of time due to void swelling from helium buildup [1].
  - Average rate of density loss after 35 years ~0.01 g/cm<sup>3</sup> per year.
  - Can vary locally for a specific sample.
  - MISC [2] was used to decay initial Pu isotopes of the 40+ year old Thor core.

[2] C. Solomon "MCNP Intrinsic Source Constructor (MISC): A User's Guide" LA-UR-12-20252 (2012)

16.15 Du-alloy Density [g/cm<sup>3</sup>] 16.10 16.05 16.00 15.95 15.90 15.85 15.80 Upper Center Idealized Jezebel 15.8 [1] R. Mulford et al. "Density Variation with Age in Delta Pu-Metal." LA-UR-03-4108 (2003)



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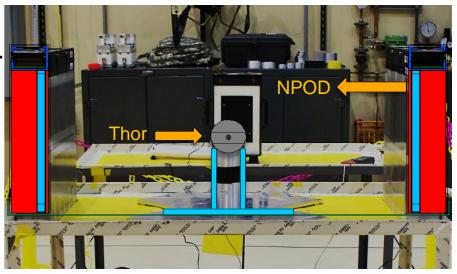
Thor Assembly

Other Assemblies

Theory

### Configuration of Thor Pu-metal core measurements.

- 14 main configurations were measured (various combinations of Thor core pieces).
- 40+ perturbation configurations:
  - Varying mass (different glory hole loadings).
  - Varying geometry (S-to-D distance).
  - Measurements with only 1 NPOD.
- 4 Detectors used:
  - 2 x NPOD (LANL neutron multiplicity detector).
  - 1 x SNAP (LANL gross neutron counter).
  - 1 x HPGe (ORTEC gamma detector).
- List-mode data obtained from NPOD measurements and simulations with MCNP
  - Hage-Cifarelli formalism of the Feynman varianceto-mean method was used in analysis.
  - Single value for efficiency (all bare configurations).
    - Measured using a neutron source: 0.0091 +/- 0.0005
    - Validated using a combination of the SNAP/NPOD count rates for each configuration.













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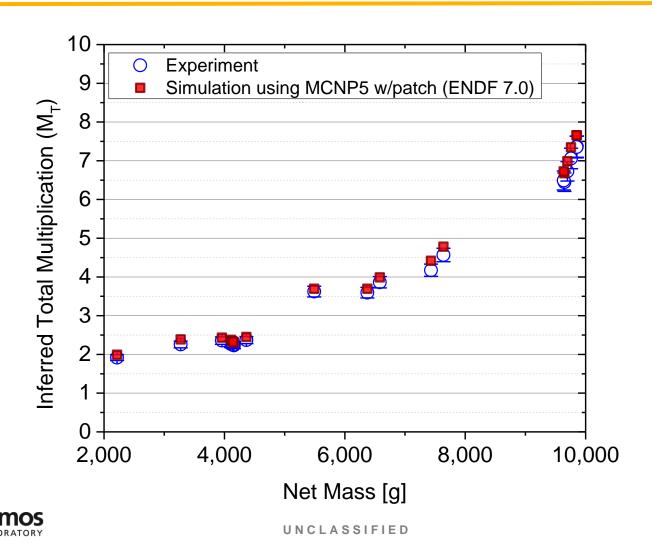
## Table of the different configuration perturbations.

			Thor Core			Glory Hole			NPOD	
CONFIG. #	PERT.	Lower	Center	Upper	$\rightarrow$	Loading	Mass [g]	Direction	S/D [cm]	#
1		+			def=vertical	None	0	def=NE-SW ⊅	def=50	def=2
2			+		def=vertical	None	0	def=NE-SW ⊅	def=50	def=2
3			+		def=vertical	Full	206.9	def=NE-SW ⊅	def=50	def=2
	3p1		+		def=vertical	Full	206.9	N-S \$	def=50	def=2
	3p2		+		def=vertical	Full	206.9	E-W ↔	def=50	def=2
	3p3		+		def=vertical	Full	206.9	def=NE-SW ⊅	49.5	def=2
	3p4		+		def=vertical	Full	206.9	def=NE-SW ⊅	49	def=2
	3p5		+		def=vertical	Full	206.9	def=NE-SW ⊅	48	def=2
	3p6		+		def=vertical	Full	206.9	def=NE-SW ⊅	45	def=2
	3p12		+		def=vertical	Quarter	49	def=NE-SW ⊅	def=50	def=2
	3p13		+		def=vertical	Altern. Full	200.7	def=NE-SW ⊅	def=50	def=2
	3p15		+		def=vertical	1/8th	24.7	def=NE-SW ⊅	def=50	def=2
	3p16		+		def=vertical	1/16th	11.8	def=NE-SW ⊅	def=50	def=2
	3p17		+		def=vertical	Full	206.9	$E-W \leftrightarrow$	def=50	def=2
4				+	def=vertical	None	0	def=NE-SW ⊅	def=50	def=2
5		+	+		def=vertical	None	0	def=NE-SW ⊅	def=50	def=2
6		+	+		def=vertical	Full	206.9	def=NE-SW ⊅	def=50	def=2
7		+		+	def=vertical	None	0	def=NE-SW ⊅	def=50	def=2
	7p1	+		+	inverted ↓	None	0	def=NE-SW ⊅	def=50	def=2
8			+	+	def=vertical	None	0	def=NE-SW ⊅	def=50	def=2
9			+	+	def=vertical	Full	206.9	def=NE-SW ⊅	def=50	def=2
10		+	+	+	def=vertical	None	0	def=NE-SW ⊅	def=50	def=2
	10p1	+	+	+	def=vertical	None	0	$E-W \leftrightarrow$	def=50	def=2
	10p2	+	+	+	def=vertical	None	0	N-S \$	def=50	def=2
11		+	+	+	def=vertical	Full	206.9	def=NE-SW ⊅	def=50	def=2
	11p2	+	+	+	def=vertical	1/16th	11.8	def=NE-SW ⊅	def=50	def=2
	11p3	+	+	+	def=vertical	Alt. Full	200.7	def=NE-SW ↗	def=50	def=2
	11p4	+	+	+	def=vertical	Full	206.9	N-S \$	def=50	def=2
	11p5	+	+	+	def=vertical	Full	206.9	$E-W \leftrightarrow$	def=50	def=2
	11p6	+	+	+	def=vertical	Full	206.9	def=NE-SW ⊅	49.5	def=2
	11p7	+	+	+	def=vertical	Full	206.9	def=NE-SW ⊅	49	def=2
	11p8	+	+	+	def=vertical	Full	206.9	def=NE-SW ⊅	48	def=2
	11p9	+	+	+	def=vertical	Full	206.9	def=NE-SW ⊅	45	def=2
	11p14	+	+	+	inverted ↓	Full	206.9	def=NE-SW ⊅	def=50	def=2
	11p15	+	+	+	def=vertical	Full	206.9	def=NE-SW ⊅	def=50	1
12		+	+	+	def=vertical	Half	109.5	def=NE-SW ⊅	def=50	def=2
13		+	+	+	def=vertical	Quarter	49	def=NE-SW ↗	def=50	def=2
14					def=vertical	Full	206.9	def=NE-SW ⊅	def=50	def=2
	14p1				def=vertical	Full	206.9	N-S ↓	def=50	def=2
	14p2				def=vertical	Full	206.9	$E-W \leftrightarrow$	def=50	def=2
	14p3				def=vertical	Half	109.5	def=NE-SW ⊅	def=50	def=2
	14p4				def=vertical	Quarter	49	def=NE-SW ↗	def=50	def=2
	14p5				def=vertical	Altern. Full	200.7	def=NE-SW ⊅	def=50	def=2



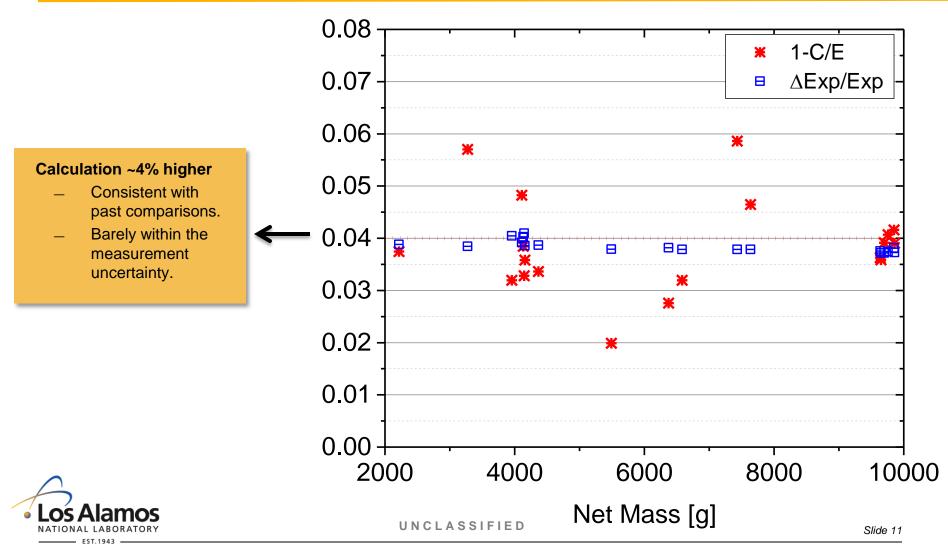


## **Total Neutron Multiplication (Inferred) vs System Mass**

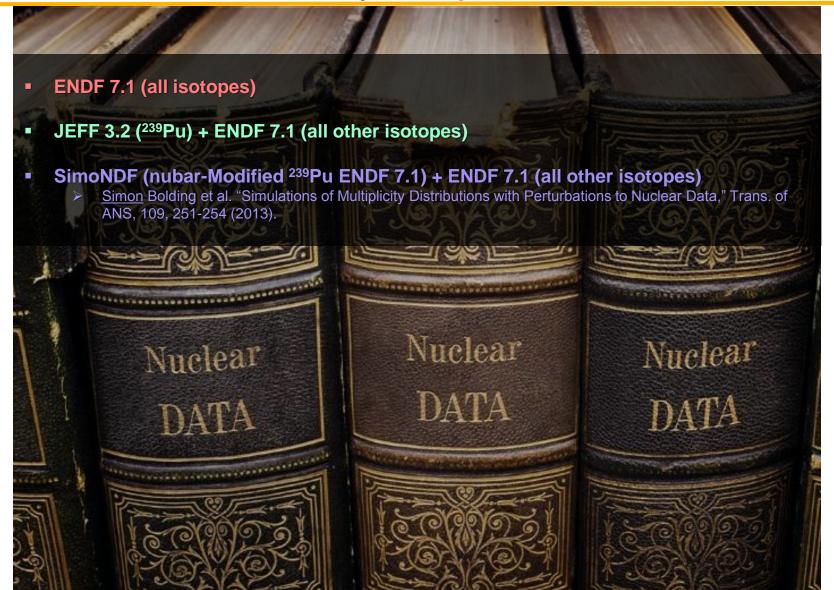




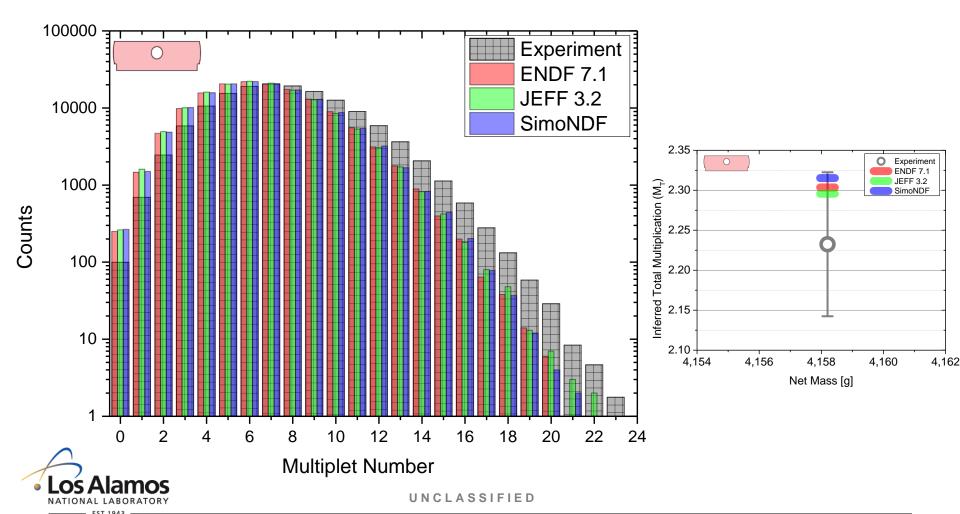
## **Calculation/Experiment for Total Multiplication**



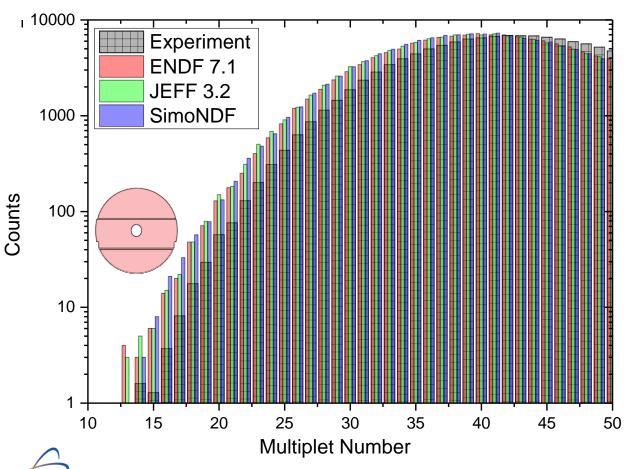
## <sup>239</sup>Pu Nuclear Data Library Comparisons

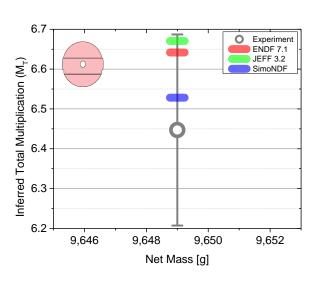


## <sup>239</sup>Pu Nuclear Data Library Comparisons



## <sup>239</sup>Pu Nuclear Data Library Comparisons



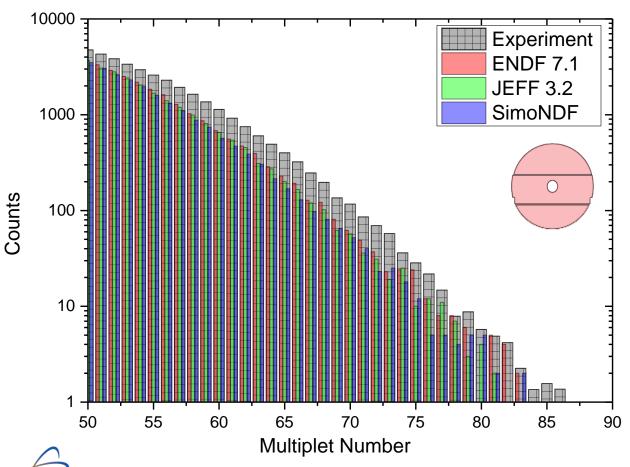


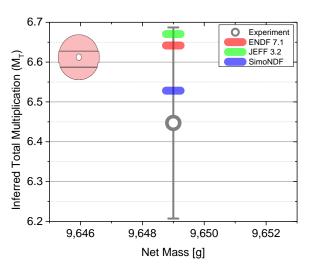


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## **Nuclear Data Library Comparisons**







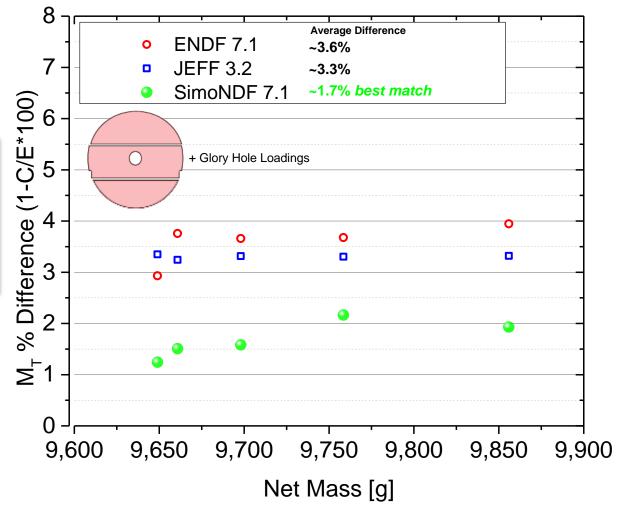
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### **Nuclear Data Library Comparisons**

#### Full assembly + loadings

- "SimoNDF" is the clear best match.
- JEFF 3.2 is a slightly better match than ENDF 7.1.



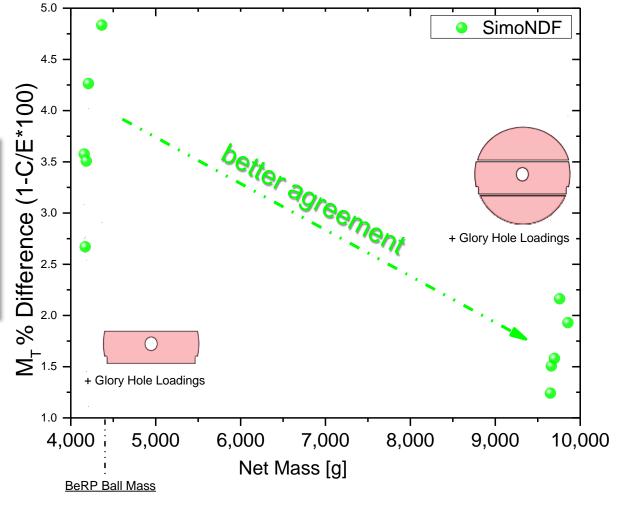


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### **Nuclear Data Library Comparisons**

#### Modified ENDF7.1 "SimoNDF"

- Correction to nubar based on BERP Ball (mass ~4500 g).
- Thor simulations with SimoNDF show better agreement at higher multiplication.

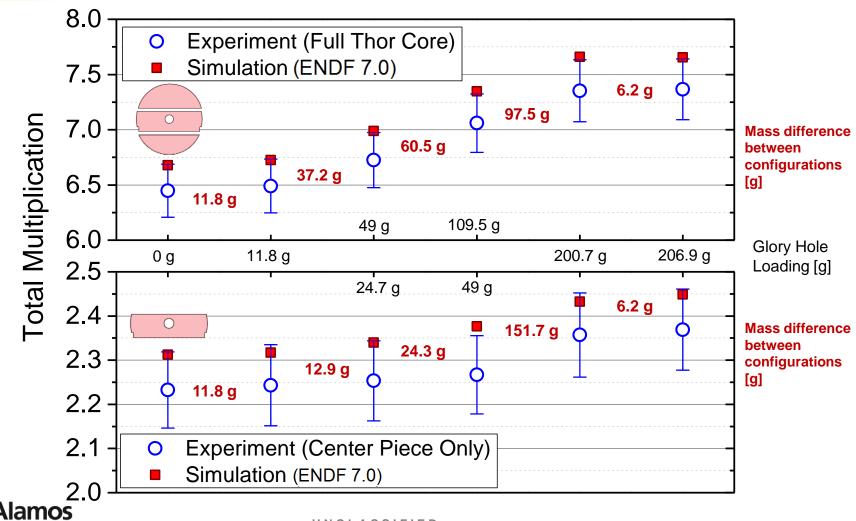




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# Detectable mass threshold decreases as mass (and system multiplication) increases.



# Varying NPOD position provides an observable effect on the inferred neuron multiplication.

#### Varying the Source-to-Detector distance.

Efficiency of stationary NPOD increases as varying NPOD moves closer.

#### Shifted NPOD (5 cm):

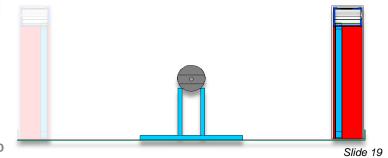
- Simulation: **27%** ↑ in R1, **75%** ↑ in R2
- Experiment: 25% ↑ in R1, 41% ↑ in R2

#### Stationary NPOD:

- Simulation: **0.85%** ↑ in R1, **2.5%** ↑ in R2
- Experiment: 0.94% ↑ in R1, 2.5% ↑ in R2

#### Removing NPOD

- Presence of an NPOD adds reflection that another NPOD can see.
- Simulation: 4.4% ↑ in multiplication
- Experiment: 3.9% ↑ in multiplication





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## Deducing the possible sources of uncertainty/bias in the simulation results.

#### Underlying nuclear data

 Analysis of detector count rates of Pu-metal systems suggests that inferred subcritical multiplication is very sensitive to fast nubar of Pu-239.

#### Thor system specifications

- Geometry re-evaluation performed.
- Isotopic composition.

#### Modeled NPOD efficiency

- Overestimate of gas pressure or active length could lead to higher inferred values\*.
- Improved efficiency measurements underway (for BeRP experiment with identical setup).

### Radiation transport code

- Computational transport codes will always have some limitations.
- MCNP6 expected to provide improved physics relative to this application.

E. C. Miller et al. "Computational Evaluation of Neutron Multiplicity Measurements of Polyethylene-Reflected Plutonium Metal," Nucl. Sci. and Eng. 176(2), 167-185 (2014).

R. Evans et al. "Sensitivity Analysis and Data Assimilation in A Subcritical Plutonium Metal Benchmark," Nucl. Sci. and Eng. 176(3), 325-338 (2014).

R. Evans, J. Li, J. Mattingly, "Adjoint Sensitivity Analysis in a Large-Scale Subcritical Plutonium Benchmark," Trans. of ANS 108, 487-490 (2013).

S. Bolding et al. "Simulations of Multiplicity Distributions with Perturbations to Nuclear Data," Trans. of ANS, 109, 251-254 (2013).

# Comparing experiments and simulations helps in assessing/reducing uncertainties in models and data.

 Ongoing effort to accurately quantify uncertainty in neutron multiplication inference from measurements and calculations.

#### Significant improvements will depend on:

- Performing these types of measurements/simulations.
- Proper documentation, for example:

B. Richard, J. Hutchinson, "Nickel-Reflected Plutonium-Metal-Sphere Subcritical Measurements" Intl. Handbook of Evaluated Criticality Safety Benchmark Experiments
NEA/NSC/DOC/(95)03/I, FUND-NCERC-PU-HE3-MULT-001(2014)



- Incremental improvements in computational tools.
- Leveraging community-wide parallel efforts related to quantifying uncertainties and correlations for nuclear data.
- Applying new analyses techniques.
  - e.g. Bayesian interpretation of historical benchmark data.





## **Acknowledgements**

This work was supported by the Nuclear Criticality Safety Program, funded and managed by the National Nuclear Security Administration for the Department of Energy.









## **Questions?**





