## Presented at the NCSD 2013, Wilmington, NC USA, September 29 - October 3, 2013

# The development and preliminary V&V of the MOC transport module in new lattice code LATC

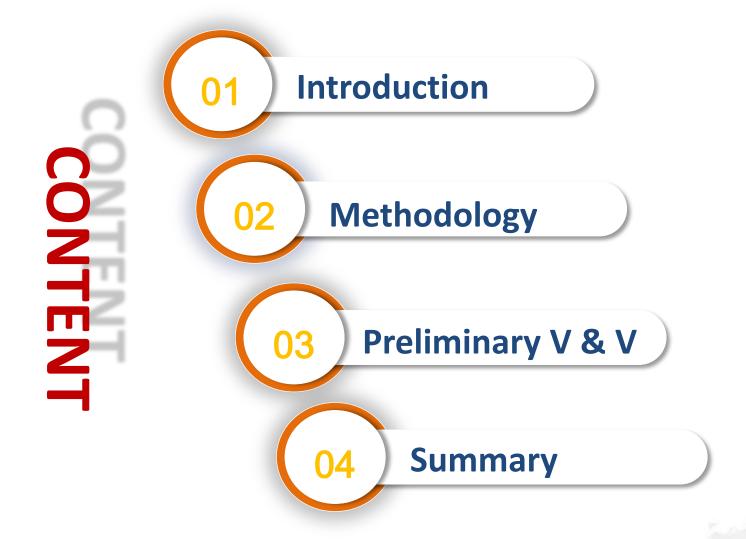
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## Introduction of SNPSDC



- > Founded in May 2010, a subsidiary of SNPTC
- Take the leading role in the State Energy Key
  Lab of NPP software (proved by DOE of
  China in Sep, 2011)
- ➤ The sole state energy key lab specialized in self-reliance NPP
- > >80 staff and 13 in reactor physics division







NPP design codes self-reliance R&D



02

04

Management, maintenance &technical support for the 3rd generation of NPP software

## **Main Business**

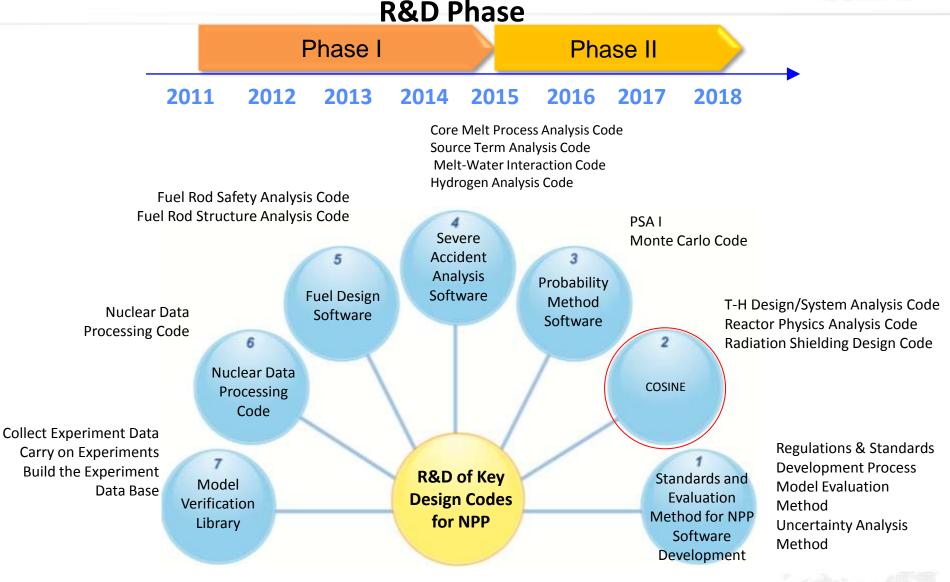
03

**V&V** technologies research for NPP software

The research on engineering application of advanced simulation technologies



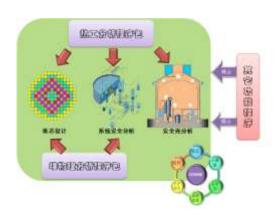






## **COSINE**

<u>COre and System IN</u>tegrated <u>Engine</u> for design and analysis



- An integrated platform
- ✓ Modular code system
- ✓ Multi-physics, multi-scale
- Sensitivity/Uncertainty analysis
- ✓ User friendly GUIs
- ✓ Parallel computations
- ✓ Software engineering QA
- **√** .....

#### THERMAL CODE

- Subchannel code(SUBC)
- ■System code (SYST)
- ■Containment code(CONT)

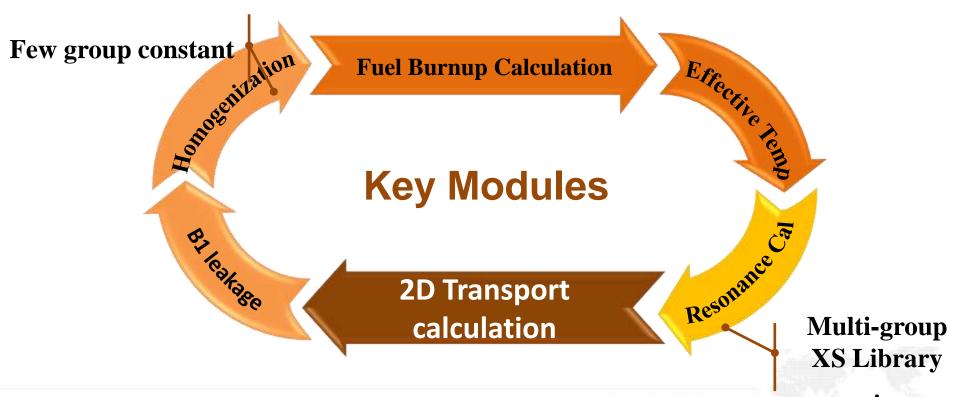
#### **PHYSICS CODE**

- *Lattice code(LATC)*
- Core code (CORE)
- ■Kinetics code(KIND)

### **LATC**



- **✓** A multi-group two-dimensional lattice transport code.
- ✓ Mainly used on PWR assemblies or pin cells.
- ✓ Capable of satisfying most of the needs for PWR lattice analysis.



## **Multi-group XS Library of LATC**



#### Present

- WIMSD-IAEA 69/172
- Published by IAEA in WLUP
- Adding the burn-up data of Wolfram isotope

## Future

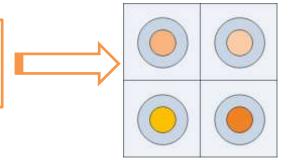
- A more accuracy library on develop
- Energy Structure: SHEM281

Total Group	Total Nuclide	Fission	Resonance
No.	No.	Product No.	Nuclide No.
281	176	85	20

## **Effective Temperature Calculation in LATC**



Temperature Distribution



#### IN

- Linear heating rate
- moderator temperature
- flow rate
- material conductance

Steady State Heat Equation

#### **OUT**

- Clad, fuel effective temperature interpolation table
- Depend on the burn up

#### Resonance Calculation in LATC



Intermediate Resonance Method



Spatially
Dependent
Dancoff
Method

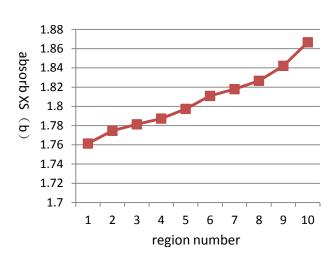
- •fuel pin radial distribution
  - effective XS
  - •power
  - nuclide density
  - •burnup
  - •...

#### **IRM**

- •2-term rational approximation
- •only one resonance region

#### **SDDM**

- •Stoker/Weiss Technique
- •fuel can be subdivided



**Equivalence theory** 

## **Burn-up Calculation Method of LATC**



#### **Predictor-Corrector Method**

**Burn-up Equation Solving:** 

- •The matrix exponential method
- Effective for stiffequation
- Bigger burn-up Step

## **Gadolinium Depletion**

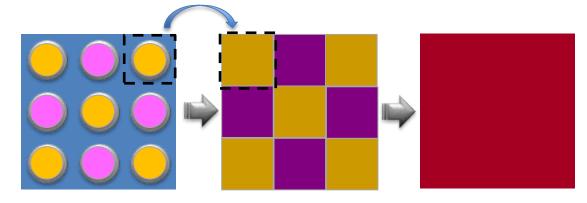
Projected PC method

Log Linear Rate Method

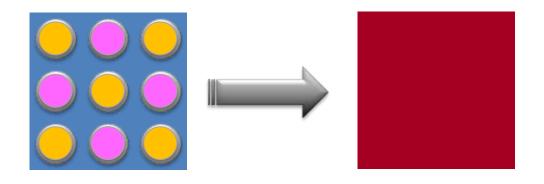
## **Transport Method of LATC**



◆ Traditional two-step scheme: CP + SN



◆ One-step scheme : MOC



## **MOC General Theory**



The transport equation can be written in the following discretised form:

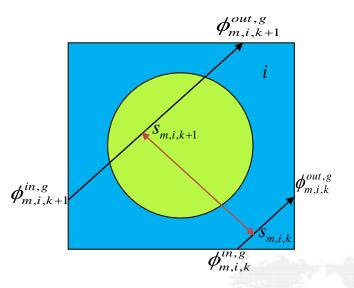
$$\frac{d\phi_{m,i}^g}{ds_m} + \sum_{tr,i}^g \phi_{m,i}^g = Q_{m,i}^g$$
 Eq (1)

The outgoing angular flux along the path k in i mesh can be given by:

$$\phi_{m,i,k}^{out,g} = \phi_{m,i,k}^{in,g} \exp(-\Sigma_{tr,i}^{g} s_{m,i,k} / \sin \theta_{m}) + \frac{Q_{m,i}^{g}}{\Sigma_{tr,i}^{g}} \left[ 1 - \exp(-\Sigma_{tr,i}^{g} s_{m,i,k} / \sin \theta_{m}) \right] \quad \text{Eq (2)}$$

The average angular flux can be obtained by integrating the Eq (2) along the path k:

$$\overline{\phi}_{m,i,k}^{g} = \frac{Q_{m,i}^{g}}{\sum_{tr,i}^{g}} + \frac{\phi_{m,i,k}^{in,g} - \phi_{m,i,k}^{out,g}}{\sum_{tr,i}^{g} S_{m,i,k}} \quad \text{Eq (3)}$$

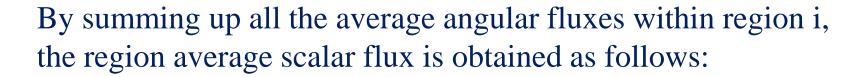


## **MOC General Theory**



The average mesh angular flux is given by:

$$\overline{\phi}_{m,i}^{g} = \frac{\sum_{k} \overline{\phi}_{m,i,k}^{g} S_{m,i,k} \delta A_{m}}{\sum_{k} S_{m,i,k} \delta A_{m}}$$
 Eq (4)



$$\overline{\phi}_i^g = \sum_m \overline{\phi}_{i,m}^g w_m \qquad \text{Eq (5)}$$

## **Ray Tracing**



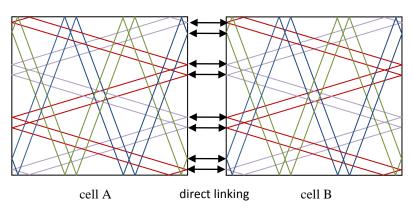
## **Modular Ray Tracing**

- MOC ray tracing process often takes large memory storage to save the neutron path information.
- Fortunately, in PWR core, many assembly have the same types and the number of types is not very large.
- In order to make the ray tracing be modular, each type of cell has its own neutron path information, and the path of every cell is associated with other's path

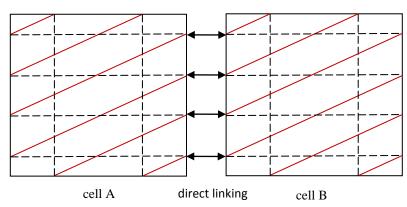
## Two modular ray tracing in LATC



DNPL technique (Direct Neutron Path Linking)



CMRT technique (Cell Modular Ray Tracing)



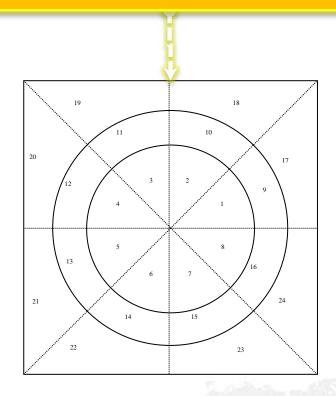
Both of the two schemes can make sure that each neutron flight path of a cell is linked to a corresponding path of the neighboring cell in order to perform a continuous characteristics calculation along the path through the cell interface.

## Meshing



- Each cell in the problem needs to be broken into numbers of sub-regions.
- ➤ In the every sub-region, the source and flux are existed and flat.
- ➤ In this way, it lends itself to an easy calculation of true areas for each mesh.

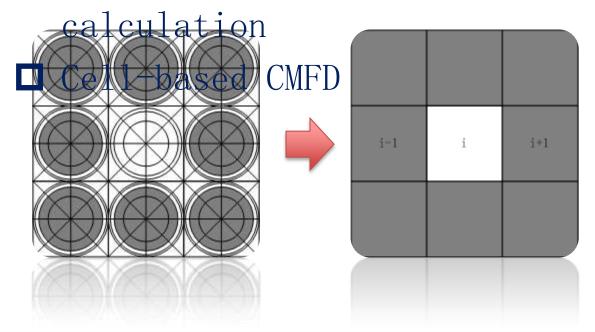
#### subdivided into octants areas.



#### **Acceleration Method CMFD**



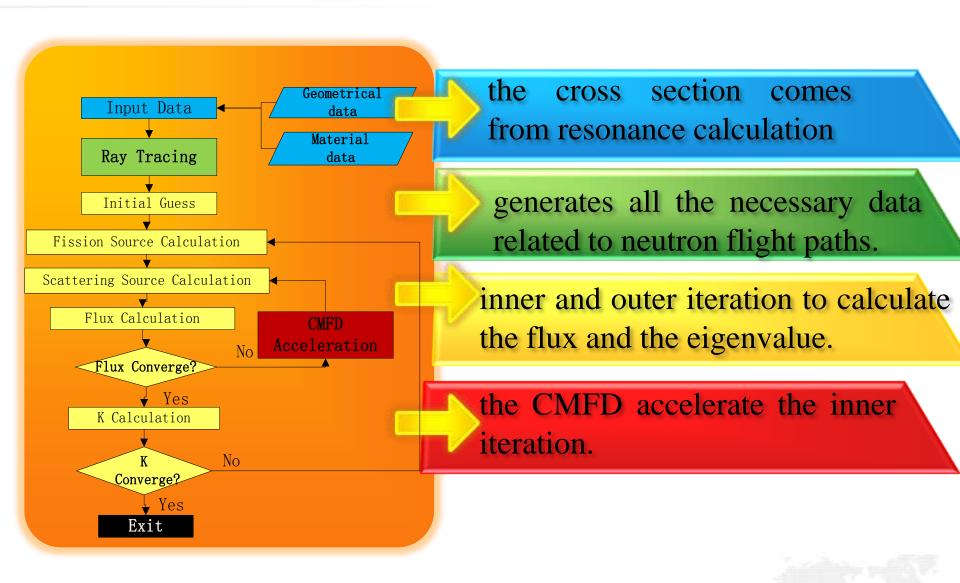
- The Coarse Mesh Finite Difference acceleration solver is implemented in LATC.
- It has been successful in reducing the computational burden for MOC transport





## **Transport Calculation Flow**





## **Validation and Verification**



- □ V&V are part of the development process and with the quality assurance (QA) process.
- □V&V are means by which the LATC is checked, and by which its performance is demonstrated and assured to be a correct interpretation of the requirements.

## Critical Experimental Benchmark



#### **LATC Versus WIMSD code**



UME-LW-AECL—aecl\_um
A uranium metal critical experimental
benchmark of AECL Laboratory.

DESIGNABLE OF ALC L LADOTATORY

Pitch (cm)	5.359	
Lattice geometry	Square	
Water/fuel volume ratio	2.305	
Moderator	H2O	
Fuel material	U-met (0.714 wt% U- 235)	
Fuel Density (g/cm3)	18.95	
Radius of fuel rods (cm)	1.6255	
Clad material	Al	
Clad Density (g/cm3)	2.6999	
Outer radius of clad (cm)	1.7475	
Thickness of clad (cm)	0.102	
Temperature (all components) (K)	293.0	
Experimental buckling B2 (cm-2)	-0.00193 ± 0.00008	

## eigenvalue result

• Under the condition of using the same iaea library.

using the same laca library.

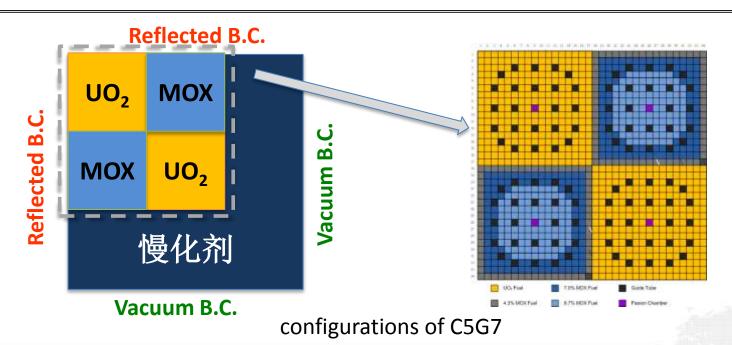
Code	eigenvale	Error
WIMSD-5B	1.00259	
LATC	1.00323	64pcm

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## Comparison against C5G7 Benchmark



- ☐ The C5G7 benchmark is proposed by OECD/NEA for deterministic Transport calculation without spatial homogenization.
- ☐ The benchmark geometry is the sixteen assembly(quarter core symmetry) C5 MOX fuel assembly problem.
- $\blacksquare$  Each fuel assembly is made up of a17  $\times$  17 lattice of square pin cells.



#### **LATC Versus MCNP**



#### The result of C5G7 benchmark

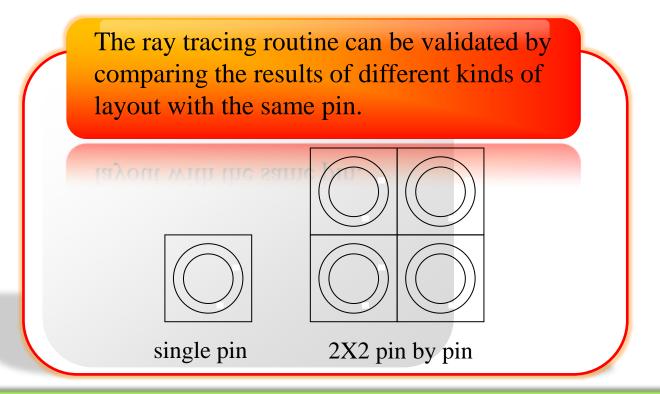
	Reference MCNP	LATC	error
Eigenvalue	1.18655	1.18744	89 pcm
Max pin power	2.498	2.502	0.16%
Min pin power	0.232	0.233	0.42%
inner UO <sub>2</sub>	492.8	493.4	0.12%
MOX assembly	211.7	211.5	0.09%
outer UO <sub>2</sub>	139.8	139.5	0.21%

#### CMFD acceleration effect:

	LATC(CMFD)	LATC(no CMFD)	error	Accelerate rate
Eigenvalue	1.18744	1.18741	3 pcm	
Calculation time	693 s	22665 s		32.7



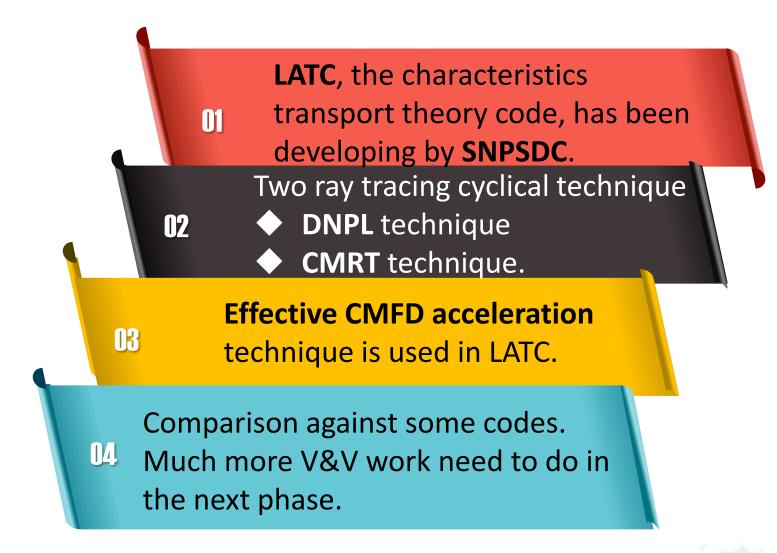




- ☐ The pin by pin calculation results are fully coincided with the single pin calculation result.
- □ It proves that the angular fluxes at the pins interfaces are correctly transferred between pins.

## **Summary & outlook**







## Thank you for your attention!



