

# NCSD Hand Calculations Workshop

Jerry Hicks

James Bunsen

# Overview

- Why Hand Calculations
- Choosing the Right Method
- Single Unit Methods
  - Diffusion Theory
  - Buckling
  - Core Density Conversions
- Array Methods
  - Surface Density
  - Density Analog
  - Limiting Surface Density
  - Solid Angle

# Why Hand Calculations

- Develop Intuition in New Analysts
- Used to Support Evaluations
- Useful for Scoping Calculations & Critical Estimates
- Must be Verified and Validated

# Choosing the Right Single Unit Method

- Diffusion
  - Large, Homogeneous Systems
  - Problems with Boundaries, Small Systems, & Absorption
- Buckling Conversions
  - Convert Between Simple Geometric Shapes
  - Requires Similar Leakage Characteristics
- Core-Density Conversions
  - Homogeneous, Critical Systems With Uniform Volume/Density Changes
  - Bare or Reflected Systems

# Diffusion Theory

- Steady State
- $B_m^2$  – Material Buckling
  - Function of Absorption and Fission Cross Sections
- $B_g^2$  – Geometric Buckling
  - Leakage of the System

$$-(-D\nabla^2\phi) - \Sigma_a\phi + v\Sigma_f\phi = \frac{1}{v} \frac{d\phi}{dt}$$

$$B_m^2 = \left( \frac{v\Sigma_f - \Sigma_a}{D} \right) \text{ and } B_g^2 = \left( \frac{\pi}{2X'} \right)^2$$

$$B_m^2 = B_g^2 \text{ then } k = 1 \text{ (Critical),}$$

$$B_m^2 > B_g^2 \text{ then } k > 1 \text{ (Supercritical),}$$

$$B_m^2 < B_g^2 \text{ then } k < 1 \text{ (Subcritical).}$$

# Buckling Conversions

- Derived From Diffusion Equation
- Used to Equate One Critical Shape to Another

Sphere: Radius-r

$$\left(\frac{\pi}{r+d}\right)^2$$

Cylinder: Radius-r, Height-h

$$\left(\frac{2.405}{r+d}\right)^2 + \left(\frac{\pi}{h+2d}\right)^2$$

Parallelepiped: Height, Width, Length

$$\left(\frac{\pi}{a+2d}\right)^2 + \left(\frac{\pi}{b+2d}\right)^2 + \left(\frac{\pi}{c+2d}\right)^2$$

Infinite Cylinder: Radius-r

$$\left(\frac{2.405}{r+d}\right)^2$$

Infinite Slab: Thickness-h

$$\left(\frac{\pi}{h+2d}\right)^2$$

Hemi-Sphere: Radius-r

$$\left(\frac{4.49}{r+d}\right)^2$$

# Core Density Conversions

- Homogeneous, Uniform Compositions
- If Reflectors Are Present: Reflector Density Changes at Same Ratio
- Relates a Critical Core With a Known Density to an **Equivalent** Critical Core With **Another** Density

**Sphere**

$$\frac{r_s}{r_{s0}} = \left( \frac{\rho}{\rho_0} \right)^{-1}$$

**Infinite  
Cylinder**

$$\frac{r_c}{r_{c0}} = \left( \frac{\rho}{\rho_0} \right)^{-1}$$

**Infinite  
Slab**

$$\frac{t}{t_0} = \left( \frac{\rho}{\rho_0} \right)^{-1}$$

# Choosing the Right Array Method

- Surface Density
  - Subcritical Center-Center Spacing in Finite Planar Array
  - Useful for Irregular Shapes
- Density Analog
  - Subcritical Center-Center Spacing in Any Array Configurations
- Limiting Surface Density ( $NB_N^2$ )
  - Center-Center Spacing in Any Array Configuration  $>64$  Units
  - Calculate Trends Due to Change in Unit Shape/Density
- Solid Angle
  - Small Numbers of Moderated Units
  - Restrictions on Single Unit Characteristics



# Surface Density

- Derived from Limiting Surface Density
- Known Information:
  - Fissile Unit Height
  - Mass of Fissile Material in Each Array Unit
  - Critical Dimensions of Infinite Water-Reflected Slab
  - Critical Mass of Unreflected Sphere of Fissile Material in Array
- Array No More Than 2 Units High
- Gives Conservative Estimate

## Surface Density Cont.

- $d$  – Center to Center Spacing
- $n$  – Number of Fissile Units  
Projected Onto a Plane
- $m$  – Fissile Material Mass (g)
- $\sigma_0$  – Surface Density Water  
Reflected Infinite Slab (g/cm<sup>2</sup>)
- $f$  – Ratio of Mass of Unit to  
Unreflected Critical Sphere
  - **MUST BE  $\leq 0.73$**

$$f = \frac{m}{m_0}$$

$$k_{eff} = \left( \frac{m}{m_0} \right)^{\frac{1}{3}} = (f)^{\frac{1}{3}}$$

$$d = \left[ \frac{nm}{0.54\sigma_0(1-1.37f)} \right]^{\frac{1}{2}} \cong 1.37 \left[ \frac{nm}{\sigma_0(1-1.37f)} \right]^{\frac{1}{2}}$$

# Density Analog

- Similar to Surface Density Method
- Used for Cubic Arrays
- Known Information:
  - Fissile Unit Height
  - Mass of Fissile Material in Each Array Unit
  - Critical Dimensions of Infinite Water-Reflected Slab
  - Critical Mass of Unreflected Sphere of Fissile Material in Array
- Array Stored in Unlimited Fashion
- Gives Conservative Estimate

## Density Analog Cont.

- $d$  – Center to Center Spacing
- $n$  – Number of Fissile Units in One Dimension (Total Units  $^{1/3}$ )
- $m$  – Fissile Material Mass (g)
- $\sigma_0$  – Surface Density Water Reflected Infinite Slab (g/cm<sup>2</sup>)
- $f$  – Ratio of Mass of Unit to Unreflected Critical Sphere
  - **SHOULD BE  $\leq 0.73$**

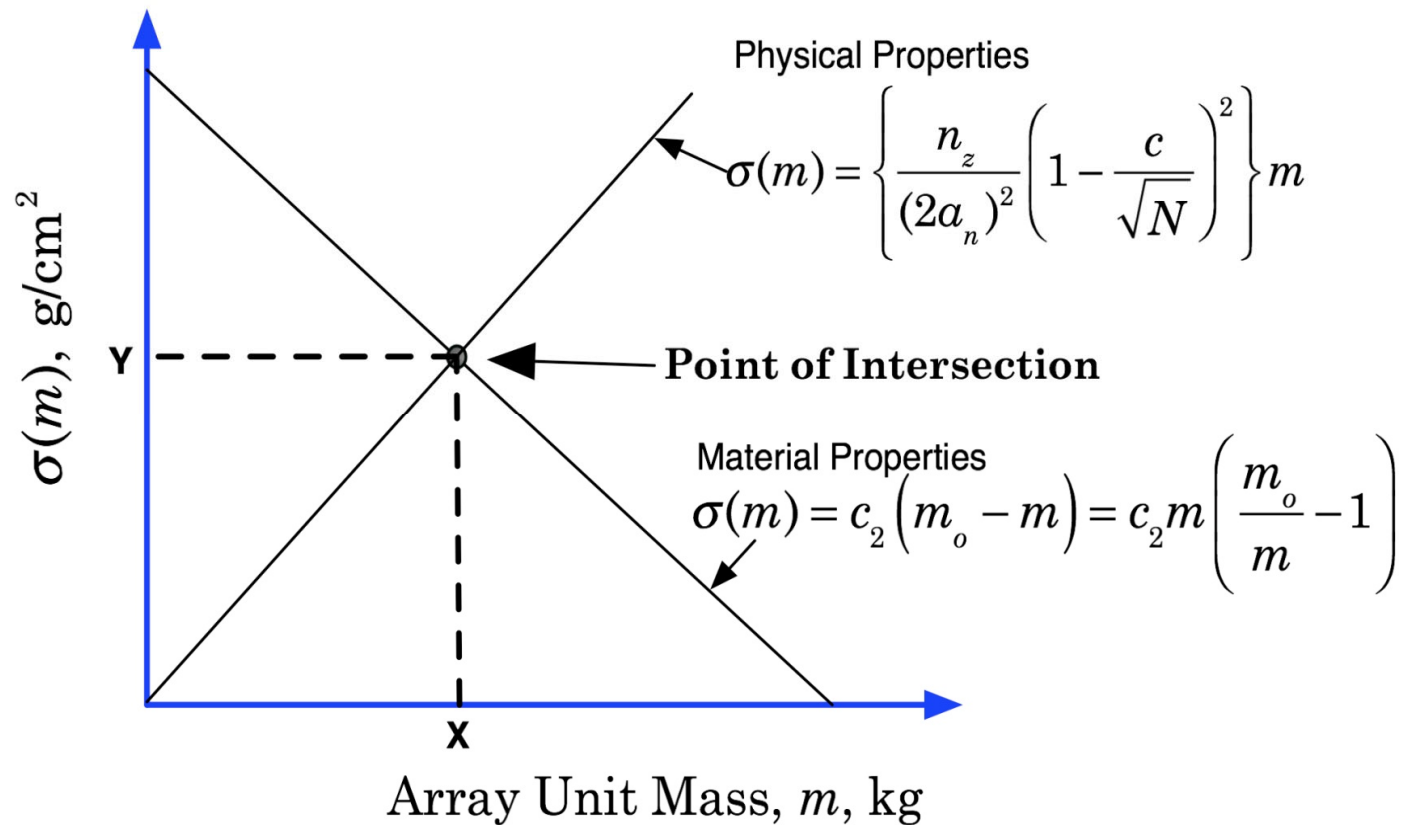
$$d = \left[ \frac{nm}{2.1\sigma_0(1-1.37f)} \right]^{\frac{1}{2}} \cong 0.69 \left[ \frac{nm}{\sigma_0(1-1.37f)} \right]^{\frac{1}{2}}$$

$$f = \frac{m}{m_0}$$

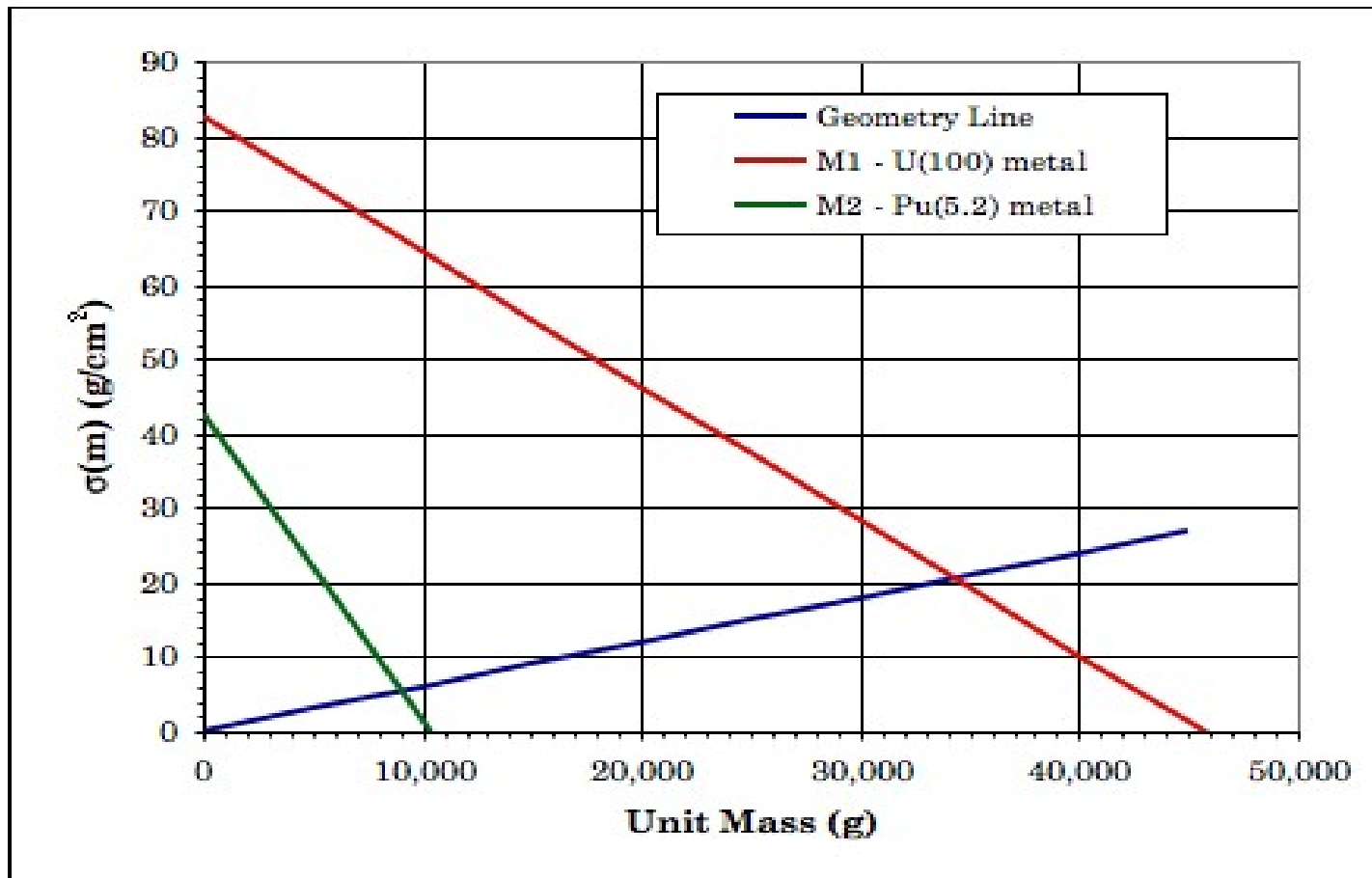
# Limiting Surface Density ( $NB_N^2$ )

- Combination of Density Analog & Diffusion Theory
  - Expands Geometric Buckling Expanded for a Cubic Array
- Known Information:
  - Fissile Unit Height
  - Mass of Fissile Material in Each Array Unit
  - Critical Mass of Unreflected Sphere
  - Characteristic Constant as Function of Material Properties ( $c_2$ )
- Can Substitute Other Fissile & Reflector Materials
- $H/X \leq 20$  &  $0.3 \leq H/D \leq 3$
- Calculates Critical Array

## Limiting Surface Density ( $NB_N^2$ ) Cont.



## Limiting Surface Density ( $NB_N^2$ ) Cont.



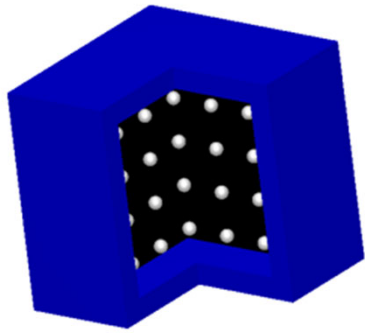
## Limiting Surface Density ( $NB_N^2$ ) Cont.

- $c_2$  – a constant that depends on all of the material properties of the arrays except for the mass,  $m$ , and is also equal to the slope of the “material-line” ( $\text{cm}^{-2}$ )
  - the Primer provides Thomas’ values for this constant for various fissile systems,
- $c$  – an empirically determined constant equal to  $0.55 \pm 0.18$  for the range of fissile materials and arrays studied by Thomas.
  - tends toward zero in a thermal system (i.e., moderated units in the array)



# Limiting Surface Density (NB<sub>N</sub><sup>2</sup>) Cont.

## Graphical Limiting Surface Density Example:



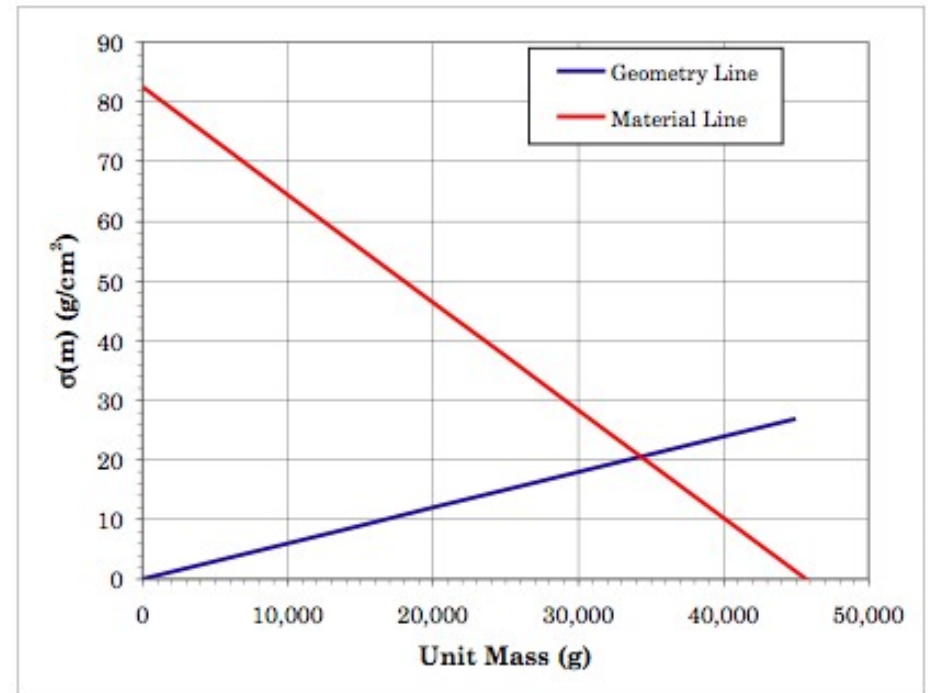
- 4x4x4 Array
- 76.2 cm (30" c-to-c spacing between units)
- U (100) metal units
- Determine unit mass for array criticality

$$\text{Geometry Line: } \sigma(m) = \frac{n_z m}{(2a_n)^2} \left(1 - \frac{c}{\sqrt{N}}\right)^2 = \frac{4m}{(2 \times 38.1 \text{ cm})^2} \left(1 - \frac{0.55}{\sqrt{64}}\right)^2$$

$$\sigma(m) = 5.974 \times 10^{-4} m \quad \text{or} \quad \frac{\sigma(m)}{m} = 5.974 \times 10^{-4}$$

$$\text{Material Line: } \sigma(m) = c_2(m_o - m)$$

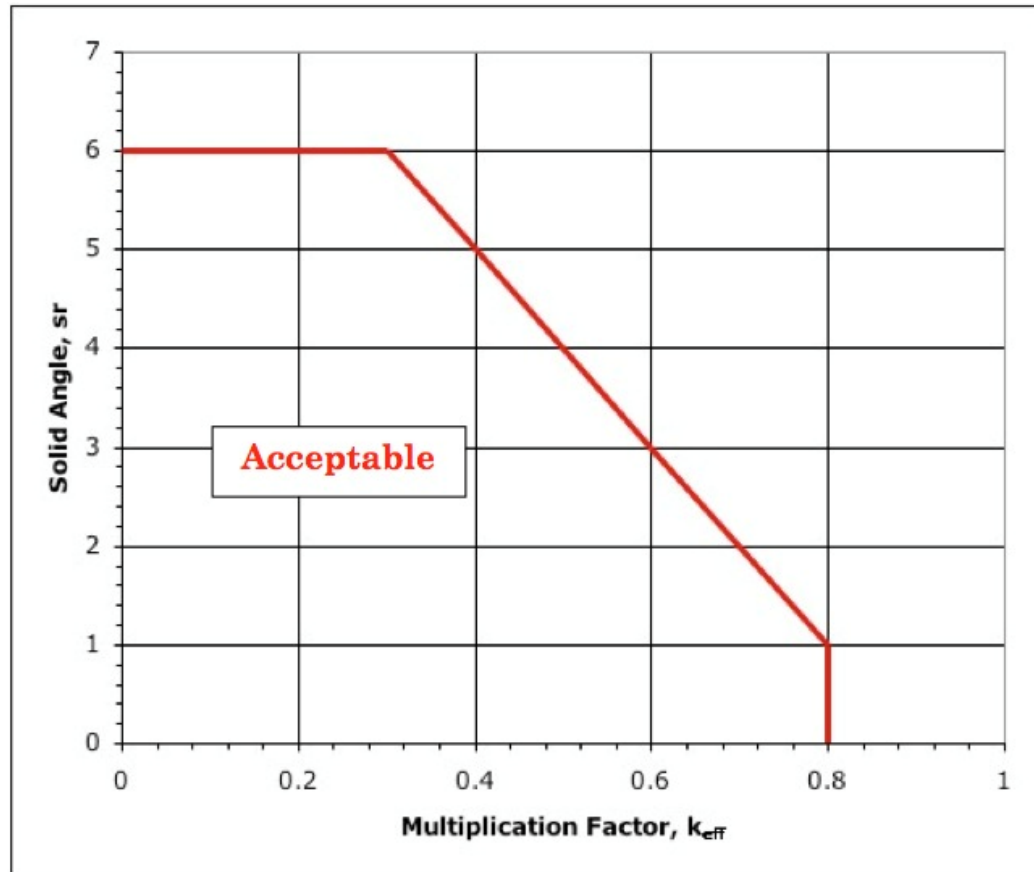
$$\sigma(m) = 1.806 \times 10^{-3} (45.68 - m) \quad \text{or} \quad \frac{\sigma(m)}{m} = 1.806 \times 10^{-3} \left(\frac{45.68}{m} - 1\right)$$



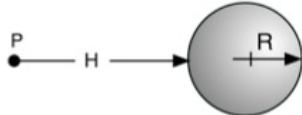
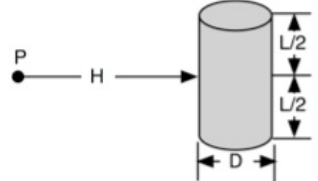
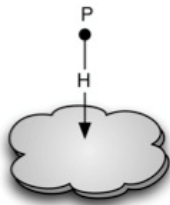
# Solid Angle

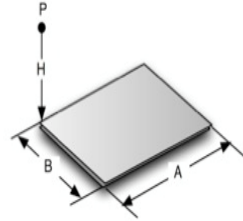
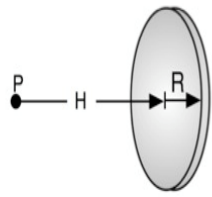
- Small Numbers of Moderated Fissile Units
- Can Be Non-Conservative for Fast Neutron Systems
- Restrictions:
  - Single Unit  $k_{\text{eff}} \leq 0.80$
  - Each Unit Subcritical with Thick Water Reflection
  - Units Must be  $\geq 0.3$  m
  - Solid Angle  $\leq 6$  Steradians
  - Reflection Must be Bound by Water

## Solid Angle Cont.



# Solid Angle Cont.

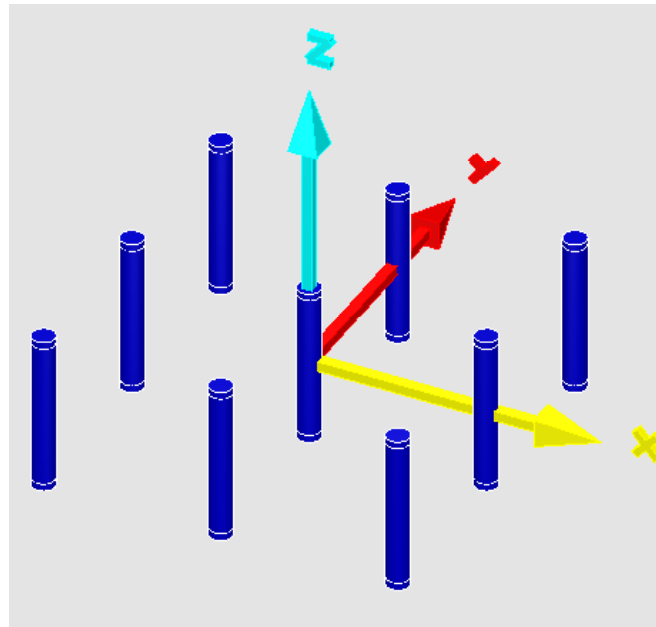
Point-to-Sphere	Point-to-Cylinder	Point-to-Arbitrary Shape
 $\Omega = 2\pi \left( 1 - \frac{1}{\sqrt{1 + (R/H)^2}} \right)$ <p>where  R = Radius of the sphere.  H = Distance from the point to the surface of the sphere.</p>	 $\Omega = \frac{LD}{H\sqrt{(L/2)^2 + H^2}}$ <p>where  L = Length of the cylinder  D = Diameter of the cylinder  H = Distance from the point to the surface of the cylinder.</p>	 $\Omega = \frac{\text{Cross Sectional Area}}{(H)^2}$

Point-to-Plane	Point-to-Disk
 $\Omega = \sin^{-1} \left( \frac{AB}{\sqrt{A^2 + H^2} \sqrt{B^2 + H^2}} \right)$ <p>where  A = Length of one side of the plane  B = Length of the other side of the plane  H = Perpendicular distance from the point to the plane.</p> <p>If the point, P, is directly above the center of the plane (not directly over a corner as shown in the figure) with dimensions <math>2A \times 2B</math>, multiply <math>\Omega</math> by 4 to obtain the solid angle.</p>	 $\Omega = 2\pi \left( 1 - \frac{1}{\sqrt{1 + (R/H)^2}} \right) \leq \frac{\pi R^2}{H^2}$ <p>where  R = Radius of the disk  H = Distance from the point P to the surface of the disk.</p>

## Solid Angle Cont.

- Problem: We want to store nine “safe”-bottles of fissile solution in a 3-by-3 array with 2-foot edge-to-edge spacing
- Question: What is the highest  $k_{eff}$  that each bottle can have as a single unit and still be subcritical in the array?

- Each bottle is 4-feet tall
- Each bottle diameter ½-foot



## Solid Angle Cont.

- Question: What unit is the most reactive unit?  
Why?

Units are 2 feet edge to edge in X and Y

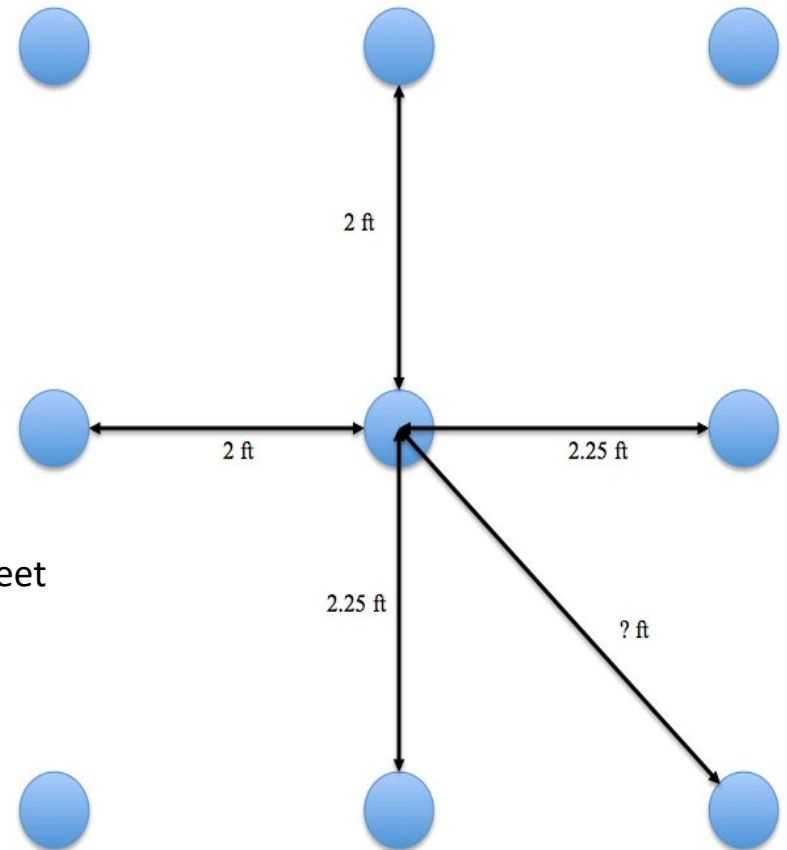
Center of central unit to edge of outer unit is  $\frac{1}{2}$  of  $\frac{1}{2}$  foot, or  $\frac{1}{4}$  foot.

Point to cylinder distance is 2 feet + 0.25 feet, or 2.25 feet

The center to center distance in X and Y is 2.5 feet.

The center to center distance on the diagonal is  $\sqrt{2.5^2}$ , or 3.54 feet

Point to cylinder distance on the diagonals is  $3.54 - 0.25 = 3.29$  feet.

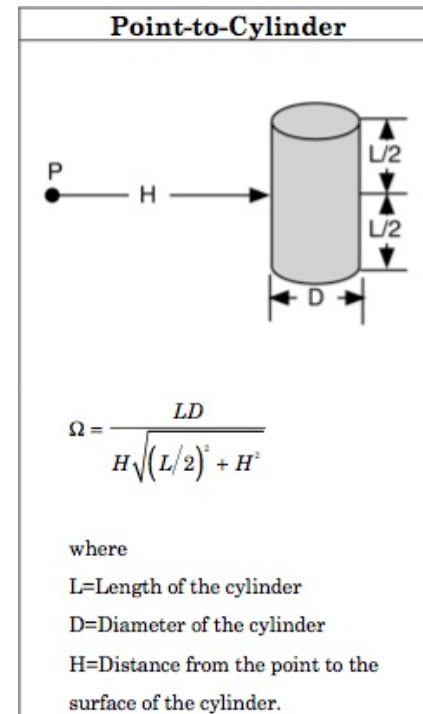


## Solid Angle Cont.

$$\bullet \Omega_n = \frac{(4 \text{ ft})\left(\frac{1}{2} \text{ ft}\right)}{2.25 \text{ ft} \left[ \left(\frac{4 \text{ ft}}{2}\right)^2 + (2.25 \text{ ft})^2 \right]^{\frac{1}{2}}} = 0.30 \text{ SR}$$

$$\bullet \Omega_f = \frac{(4 \text{ ft})\left(\frac{1}{2} \text{ ft}\right)}{3.29 \text{ ft} \left[ \left(\frac{4 \text{ ft}}{2}\right)^2 + (3.29 \text{ ft})^2 \right]^{\frac{1}{2}}} = 0.16 \text{ SR}$$

$$\Omega_{total} = 4\Omega_n + 4\Omega_f = 1.84 \text{ SR}$$



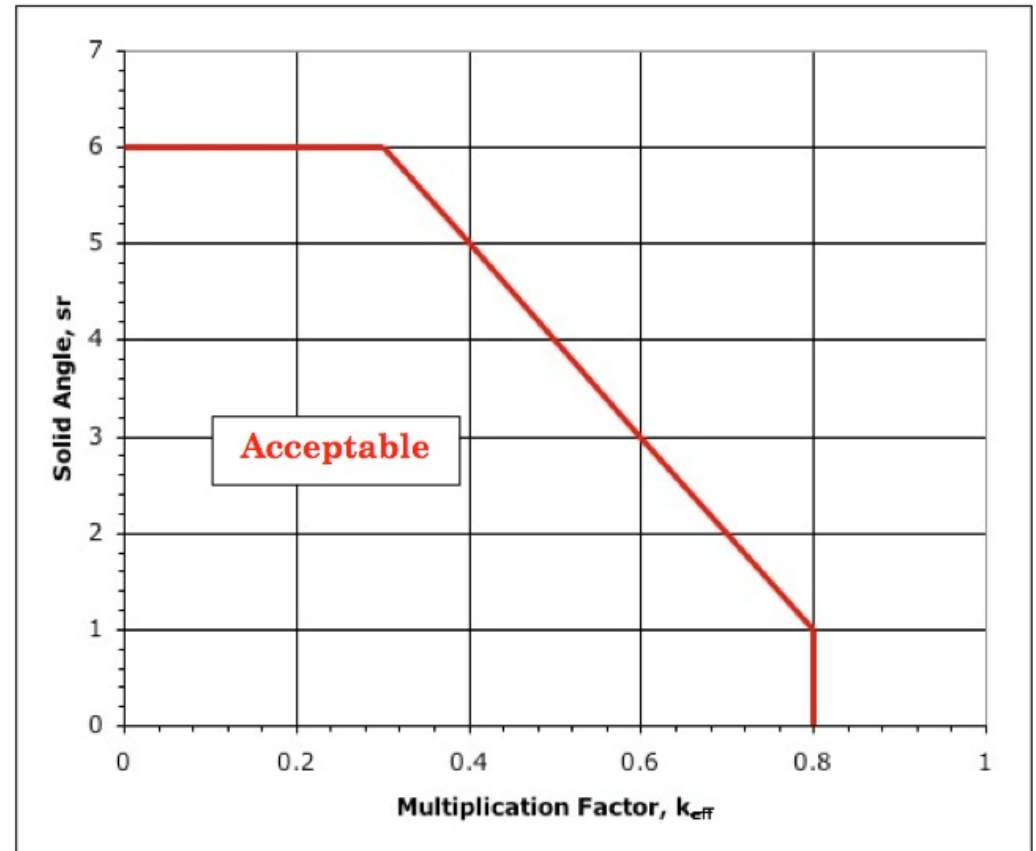
- Question: What is the highest allowed  $k_{eff}$ ?

## Solid Angle Cont.

$$\Omega_{total} = 1.84 \text{ SR}$$

$$1.84 = 9 - 10k_{eff}$$

$$k_{eff} = \left\lfloor \frac{9 - 1.84}{10} \right\rfloor = 0.72$$



What else is required?

What happens if we move the bottles closer together?



# Potential Solutions to Competition

# ANSI/ANS 8.7

- Cubic Array
- $k_{\text{eff}} < 0.95$
- 20 cm Water Reflection
- All Units are Spheres
- \*DOUBLE BATCHING  
SHALL BE CONSIDERED\*

**Table 5.7**  
**Unit Mass Limit in Kilograms of Plutonium per Cell in**  
**Water-Reflected Storage Arrays: Metal, 100 wt-%  $^{239}\text{Pu}$**

<i>Number of Units in Cubic Storage Arrays</i>	<i>Minimum Dimension of Cubic Storage Cell (mm)</i>					
	254	305	381	457	508	610
<i>(H/Pu <math>\leq 0.01</math>; Pu density <math>\leq 19.7 \text{ g/cm}^3</math>)</i>						
64	3.4	4.1	4.9	5.5 <sup>a</sup>	5.8 <sup>a</sup>	6.3 <sup>a</sup>
125	2.9	3.6	4.4	5.1 <sup>a</sup>	5.4 <sup>a</sup>	6.0 <sup>a</sup>
216	2.6	3.2	4.1	4.7	5.1 <sup>a</sup>	5.7 <sup>a</sup>
343	2.3	2.9	3.8	4.4	4.8 <sup>a</sup>	5.4 <sup>a</sup>
512	2.1	2.7	3.5	4.2	4.6	5.2 <sup>a</sup>
729	1.9	2.5	3.3	3.9	4.3	5.0 <sup>a</sup>
1000	1.7	2.3	3.1	3.7	4.1	4.8

<sup>a</sup> Values are greater than 90 % of critical spherical mass, water reflected.

## ANSI/ANS 8.7 Cont.

- 125 Units, 4.4kg/unit = 550 kg total
  - 381 mm Cells (15 in)
  - 5x5x5 Array
  - **6.9 m<sup>3</sup>**
- 216 Units, 2.6kg/unit = 561.6 kg total
  - 254 mm Cells (10 in)
  - 6x6x6 Array
  - **3.5m<sup>3</sup>**

# Surface Density

$$d = \left[ \frac{nm}{0.54\sigma_0(1-1.37f)} \right]^{\frac{1}{2}} \cong 1.37 \left[ \frac{nm}{\sigma_0(1-1.37f)} \right]^{\frac{1}{2}}$$

- Choose Mass and Unit Depth (m&n)
  - f is determined from m
- $\sigma_0$  = Critical, Infinite Slab Height \* Density ( $h_{\text{slab,crit}} * \rho$ )
  - $h_{\text{slab,crit}}$  is looked up or calculated
    - Look up: ANSI/ANS 8.1
    - Calculated with Buckling Calculations  $\left( \frac{\pi}{r+d} \right)^2 = \left( \frac{\pi}{h+2d} \right)^2$ 
      - d – Extrapolation Distance (3.28cm)
      - r – Critical Radius Sphere (Given or looked up)

## Surface Density Cont.

- Masses: 2 kg, 4.5 kg, 7 kg & Unit Depth: 1 Unit, 2 Units
    - 2.0 kg, 1 Unit:  $d = 17.6$  cm
    - 2.0 kg, 2 Unit:  $d = 25.0$  cm
    - 4.5 kg, 1 Unit:  $d = 35.3$  cm
    - 4.5 kg, 2 Unit:  $d = 49.9$  cm
    - 7.0 kg, 1 Unit:  $d = 91.9$  cm
    - 7.0 kg, 2 Unit:  $d = 130.0$  cm
- 250 Total Units
- 112 Total Units
- 72 Total Units

# Surface Density Final

- Distance between units isn't the final step
- Choose an array size:
  - 2.0 kg, 1 Unit: 1x8x32     $V=0.82 \text{ m}^3$
  - 2.0 kg, 2 Unit: 2x8x16     $V=2.12 \text{ m}^3$
  - 4.5 kg, 1 Unit: 1x4x28     $V=1.62 \text{ m}^3$
  - 4.5 kg, 2 Unit: 2x4x14     $V=5.97 \text{ m}^3$
  - 7.0 kg, 1 Unit: 1x2x36     $V=5.55 \text{ m}^3$
  - 7.0 kg, 2 Unit: 2x2x18     $V=42.7 \text{ m}^3$

$$\text{Volume} = (2r+d(x-1)) * (2r+d(y-1)) * (2r+d(z-1))$$

# Density Analog

$$d = \left[ \frac{nm}{2.1\sigma_0(1-1.37f)} \right]^{\frac{1}{2}} \cong 0.69 \left[ \frac{nm}{\sigma_0(1-1.37f)} \right]^{\frac{1}{2}}$$

- Again, choose  $n$  &  $m$  and  $\sigma_0$  consistent
- Same masses as Surface Density
- Cubic Arrays:
  - 2.0 kg ~ 6x6x6 array (6.3)
  - 4.5 kg ~ 5x5x5 array (4.8)
  - 7.0 kg ~ 4x4x4 array (4.2)

## Density Analog Cont.

- 2.0 kg: d=22.3 cm V=1.6
- 4.5 kg: d=39.6 cm V=4.6
- 7.0 kg: d=94.4 cm V=24.9

$$\text{Volume} = (2r + d(x-1))^3$$

- Problems getting the right number of units



# Conclusion

- Hand calculations have a place
- Fast, relatively easy to do
- Very conservative calculations
- Struggle with abnormal conditions
- Great for scoping and to support further calculations

Questions?